# **PUBLISHED VERSION**

Mi, J.; Antonia, R. A.; Anselmet, F..

Joint statistics between temperature and its dissipation rate components in a round jet, *Physics of Fluids*, 1995; 7(7):1665-1673.

© 1995 American Institute of Physics. This article may be downloaded for personal use only. Any other use requires prior permission of the author and the American Institute of Physics.

The following article appeared in Phys. Fluids **7**, 1665 (1995) and may be found at http://link.aip.org/link/doi/10.1063/1.868484

## **PERMISSIONS**

http://www.aip.org/pubservs/web\_posting\_guidelines.html

The American Institute of Physics (AIP) grants to the author(s) of papers submitted to or published in one of the AIP journals or AIP Conference Proceedings the right to post and update the article on the Internet with the following specifications.

On the authors' and employers' webpages:

- There are no format restrictions; files prepared and/or formatted by AIP or its vendors (e.g., the PDF, PostScript, or HTML article files published in the online journals and proceedings) may be used for this purpose. If a fee is charged for any use, AIP permission must be obtained.
- An appropriate copyright notice must be included along with the full citation for the published paper and a Web link to AIP's official online version of the abstract.

31st March 2011

http://hdl.handle.net/2440/2887

# Joint statistics between temperature and its dissipation rate components in a round jet

J. Mi and R. A. Antonia

Department of Mechanical Engineering, University of Newcastle, New South Wales 2308, Australia

#### F Anselmet

Institut de Mécanique Statistique de la Turbulence, Université d'Aix-Marseille II, 13003 Marseille, France

(Received 28 November 1994; accepted 27 March 1995)

The joint statistics between the temperature fluctuation  $\theta$  and all three components of the temperature dissipation rate  $\epsilon_{\theta}$  are investigated in the self-preserving region of a slightly heated turbulent round jet. The main factors which determine the correlation between  $\theta$  and  $\epsilon_{\theta}$  are the asymmetry of  $p(\theta)$ , the probability density function (PDF) of  $\theta$ , and the anisotropy of the small-scale turbulence. The assumption of statistical independence between  $\theta$  and  $\epsilon_{\theta}$  appears to be more closely approximated in this flow than in a turbulent plane jet. Relatedly, the assumption of local isotropy is also more closely satisfied in the round jet than in the plane jet. When  $\theta$  is in the range  $\pm 2$  standard deviations, the expectations of all components of  $\epsilon_{\theta}$ , conditioned on  $\theta$ , are approximately equal in the fully turbulent part of the flow; the magnitude of the conditional expectation is consistent with the independence assumption. © 1995 American Institute of Physics.

#### I. INTRODUCTION

The instantaneous scalar dissipation rate  $\epsilon_{\theta} \equiv \alpha(\theta_{1}^{2})$  $+\theta_2^2+\theta_3^2$ ), where  $\theta_i = \partial \theta / \partial x_i$  and  $\alpha$  is the thermal diffusivity] and its dependence on the scalar fluctuation  $\theta$  are important in turbulent combustion modeling.<sup>1,2</sup> The mean scalar dissipation rate  $\langle \epsilon_{\theta} \rangle$  (hereafter, angular brackets denote time averages) features in second-order models of turbulent flows: e.g., through the time scale ratio  $(\langle q^2 \rangle \langle \epsilon \rangle^{-1} / \langle \theta^2 \rangle \langle \epsilon_{\theta} \rangle^{-1})$ , where  $\langle q^2 \rangle$  is the average turbulent energy and  $\langle \epsilon \rangle$  is the average dissipation rate of  $\langle q^2 \rangle$ . The dependence between  $\theta$  and  $\epsilon_{\theta}$ reflects the dependence between large-scale and small-scale motions. The joint probability density function (JPDF) of  $\theta$ and  $\epsilon_{\theta}$  can be correlated to the average rate of creation or destruction of chemical species in both premixed<sup>3</sup> and diffusion<sup>4</sup> flames since the average reaction rate is proportional to the expectation of  $\epsilon_{\theta}$  conditioned on the stoichiometric value of  $\theta$ .

Measurements of  $\langle \epsilon_{\theta} \rangle$  have been made in nonreacting turbulent flows: grid turbulence,<sup>5,6</sup> a quasihomogeneous shear flow,<sup>7</sup> a self-preserving plane jet,<sup>8</sup> a self-preserving plane wake,<sup>9</sup> a turbulent boundary layer,<sup>10</sup> a developing round jet,<sup>11,12</sup> and a self-preserving round jet.<sup>13,14</sup> By contrast, however, more limited experimental data are available for the joint statistics of  $\theta$  and  $\epsilon_{\theta}$ . Iso-JPDF contours and correlations between the temperature fluctuation  $\theta$  and an approximation to the temperature dissipation rate  $\epsilon_{\theta}$  were obtained by Anselmet and Antonia<sup>15</sup> in the self-preserving region of a slightly heated turbulent plane jet. They provided approximate support for the assumption of independence between  $\theta$  and  $\epsilon_{\theta}$ . This assumption allows the JPDF,  $p(\theta, \epsilon_{\theta})$ , of these two quantities to be written as a product of the individual or marginal PDFs, viz.

$$p(\theta, \epsilon_{\theta}) = p(\theta)p(\epsilon_{\theta}). \tag{1}$$

Anselmet and Antonia<sup>15</sup> noted that Eq. (1) seemed to be more reasonably supported by the data as the distance from the jet centerline increases. Recently, using measurements of

 $p(\theta, \theta_{,i}^2)$  [unless otherwise mentioned, repeated subscripts do not imply summation] in a turbulent boundary layer and  $p(\theta, \theta_{,i}^2)$  [ $\theta_{,i} \equiv \partial \theta / \partial t$ ] in the developing region  $(x_1/d = 3 \sim 15)$  of a turbulent round jet, Anselmet  $et\ al.^{16}$  pointed out that Eq. (1) is strictly valid only when  $p(\theta)$  is symmetrical. For a symmetrical PDF, all odd-order moments are zero; in particular, the skewness  $S_{\theta} \equiv \langle \theta^3 \rangle / \langle \theta^2 \rangle^{3/2}$  is zero. These authors also noted that intermittency (as measured, for example, by the intermittency factor  $\gamma$  or fraction of the time for which the flow is turbulent) plays a much smaller role than the asymmetry of  $p(\theta)$  in determining the correlation between  $\theta$  and  $\epsilon_{\theta}$ .

While Anselmet et al.'s 16 conclusion seems reasonable, it appears to be somewhat at variance with the data of Ref. 11. Using Raman scattering, these authors measured the CH<sub>4</sub> mass fraction (identified, for the present purpose, with  $\theta$ ), two components (axial and radial) of  $\epsilon_{\theta}$  in the developing region  $(5 \le x_1/d \le 17)$  of an isothermal methane round jet. On the jet axis,  $\langle \theta_1^2 \rangle$  was approximately equal to  $\langle \theta_2^2 \rangle$ . Since  $\langle \theta_2^2 \rangle$ and  $\langle \theta_3^2 \rangle$  are equal on the axis, it follows that  $\langle \epsilon_{\theta} \rangle$  should conform approximately with isotropy there. Also, the correlation  $\langle \theta \epsilon_{\theta} \rangle$  was very nearly zero on the axis, i.e., in apparent support of (1) since  $\langle \theta \epsilon_{\theta} \rangle = \langle \theta \rangle \langle \epsilon_{\theta} \rangle = 0$  if  $\theta$  and  $\epsilon_{\theta}$  are independent. Yet,  $p(\theta)$  is not symmetrical on the axis since the available data indicate that  $S_{\theta}$  is negative. Values of  $S_{\theta}$  were not reported in Ref. 11 but previous measurements, 17-19 also in a round jet, show that  $S_{\theta}$  varies typically between -1 $(x_1/d \approx 3)$  and -0.3  $(x_1/d \approx 60)$  along the axis. As the distance  $(x_2)$  from the axis increases,  $S_{\theta}$  crosses zero and becomes positive. Yet, Namazian et al. 11 found that the magnitude of  $\langle \theta \epsilon_{\theta} \rangle$  is significantly different from zero when  $x_2 > 0$ , especially at  $x_2 \approx R_u$  (where  $R_u$  is the jet half-radius); for  $x_1/d < 17$ , their data indicated a more pronounced departure of  $\langle \epsilon_{\theta} \rangle$  from isotropy as the radial distance increased.

The preceding observations suggest that it is not clear whether the degree of correlation between  $\theta$  and  $\epsilon_{\theta}$  is caused mainly by the departure of  $p(\theta)$  from symmetry or by the

deviation of  $\langle \epsilon_{\theta} \rangle$  from isotropy or whether it is the result of both those factors. To resolve this ambiguity, we have examined the effects on  $\langle \theta \epsilon_{\theta} \rangle$  of the asymmetry of  $p(\theta)$  and the anisotropy of  $\langle \epsilon_{\theta} \rangle$  in the nearly self-preserving region of a slightly heated turbulent round jet. In this flow, Antonia and Mi<sup>13</sup> have found that local isotropy of the temperature field is closely satisfied, in the context of either the variances or spectra of  $\theta_i$ , on the axis; also, the symmetry of  $p(\theta)$  is expected to be a reasonable approximation at the point between  $x_2=0$  and  $x_2=R_u$  where  $S_{\theta}\approx 0$ . Another objective of this paper is to investigate the expectation of  $\theta_{i}^{2}$  conditioned on particular values of  $\theta$ , since such statistics are required for closing the equation for the evolution of the PDF of a passive scalar  $\theta$  in turbulent flows (e.g., Refs. 20–23). We emphasize that, for the present work, all three components of  $\epsilon_{\theta}$  are measured. In particular,  $\theta_1$  was measured directly, thus circumventing the use of Taylor's hypothesis. The present joint statistics of  $\theta$  and  $\epsilon_{\theta}$  are therefore likely to be more reliable than if only  $\theta_{,t}^2$  were available. It should be noted that the basic data set used for this paper is the same as in Ref. 13.

#### II. EXPERIMENTAL SETUP AND TEST CONDITIONS

The jet rig has an axisymmetric nozzle with a 10:1 contraction ratio. The air supply was heated by an electrical fan heater (2.4 kW) located at the blower entrance. To obtain a uniform and symmetrical (about the jet axis) mean temperature profile at the nozzle exit of diameter d=25.4 mm, the complete tunnel was insulated (25 mm thick insulating foam with a metallic foil overlay). At the nozzle exit, the temperature  $T_j$  ( $\approx$ 32 °C above ambient) was uniform within  $\pm 1\%$ . The exit velocity  $U_j$  was 11 m/s and the Reynolds number  $R_d = U_j d/\nu$ , where  $\nu$  is the kinematic viscosity, was about  $1.9 \times 10^4$ .

All measurements were made at  $x_1/d=30$  (selfpreservation was approximately reached at  $x_1/d \approx 15$ , e.g., Ref. 19) and were restricted to the nearly fully turbulent region  $(0 \le x_2/R_u \le 1)$  to avoid flow reversal and high local turbulence intensities. On the axis, the mean velocity  $U_0$  and mean temperature  $T_0$  were 2.1 m/s and 4.8 °C (relative to ambient) respectively. The turbulence Reynolds number  $R_{\lambda}$ , based on the Taylor microscale  $\lambda$  (= $U_0^{-1}\langle u_1^2\rangle^{1/2}/\langle u_{1,t}^2\rangle^{1/2}$ ), was approximately 150 and the Kolmogorov length scale  $\eta$  $[\equiv (\nu^3/\langle \epsilon \rangle)^{1/4}]$  was about 0.17 mm. The Péclet number  $P_{\lambda}$  $(\equiv \langle u_1^2 \rangle^{1/2} \lambda_{\theta} / \alpha$ , where  $\lambda_{\theta} = \langle \theta^2 \rangle^{1/2} / \langle \theta_1^2 \rangle^{1/2})$  was equal to 83. The half-radii  $R_{\mu}$  and  $R_{\theta}$ , defined on the basis of mean velocity and mean temperature profiles, were 75 and 90 mm, respectively. The ratio  $Gr/R_0^2(Gr = gR_u^3T_0/\nu T_a)$  is the Grashof number,  $T_a$  is the absolute ambient temperature,  $R_0 = U_0 R_u / \nu$  is the local Reynolds number) is about 0.0027, indicating that the effect of buoyancy is negligible and justifying the use of temperature as a passive contaminant.

Spatial instantaneous derivatives  $\theta_i$  of the temperature fluctuation  $\theta$  were obtained using two parallel cold wires. Wollaston (Pt-10% Rh) wires of nominal diameter  $d_w \approx 0.63$   $\mu$ m were operated by in-house constant current circuits supplying 0.1 mA to each wire. For this value of electrical current and for the experimental conditions outlined above, the velocity contamination of the temperature signal had a negligible effect on the statistics presented in this paper. The

wires, with a nominal length  $l_w$  of about 0.4 mm, were perpendicular to the flow direction. Each wire was carefully checked under a microscope for straightness immediately prior to the experiments. Care was taken to ensure that the etched portion of each wire was central and parallel so as to minimize the uncertainty in the measurement of  $\Delta x_i$ , the separation in the  $x_i$  direction between the wires. Following a detailed investigation  $^{24}$  of the effect of  $\Delta x_i$  on  $\theta_{,i}$ , the separation  $\Delta x_i$  was chosen equal to about  $3\eta$  since, for this value of  $\Delta x_i$ , the correction which had to be applied to obtain reliable values of  $\langle \theta_{,i}^2 \rangle$  was relatively small. Also, this value of  $\Delta x_i$  is sufficiently large to avoid the large uncertainty due to the electronic noise.  $^{25}$ 

The diameter  $d_w$  and length  $l_w$  of the wires were chosen so that the ratio  $l_w/d_w$  ( $\approx$ 700) was sufficiently large to avoid possible attenuation at low wave numbers<sup>26</sup> while the ratio  $l_w/\eta$  was as small as practicable. At  $x_1/d=30$  and  $x_2/R_u=0$ , the value of  $l_w/\eta$  ( $\approx$ 2.6) was small enough to avoid making a wire length correction (Wyngaard's<sup>27</sup> calculations show that for a wire length of about  $3\eta$ ,  $\langle \epsilon_{\theta} \rangle$  is attenuated by about 10%). Only the central part of the Wollaston wires was etched to avoid difficulties associated with fully etched wires. For a given wire length, Paranthoen et al. 26 found that the signal for a fully etched wire is more attenuated than that from a partially etched wire. Estimates of the temperature coefficient of the cold wires were made by mounting both wires at the jet exit using a 10  $\Omega$  platinum resistance thermometer operated in a Leeds and Northrup 8087 bridge (with a resolution of 0.01 °C).

The cutoff frequency  $f_c$  of the low-pass filter was selected by viewing the time derivative spectra on the screen of a real-time spectrum analyser (HP3582A). Special attention was given to the degree of correlation between the two signals and to the time derivative spectra of these signals. If the spectra looked different, one or both of the wires were replaced by newly etched ones until there was no discernible difference. The values of  $f_c$  were identified with the frequencies at which the derivative spectra were about 2-3 dB higher than those corresponding to the frequencies at which electronic noise first became important. These settings were determined at each measurement location and found to be the same for the two wires. At  $x_2=0$  and  $x_2=R_u$ ,  $f_c$  was 2.2 and 1.2 kHz, respectively, while the Kolmogorov frequency  $f_k$  $(=\langle U_1 \rangle/2\pi\eta, \langle U_1 \rangle)$  is the local mean streamwise velocity was about 2.0 and 0.8 kHz.

After filtering, the signals from the two wires were passed through buck and gain units to offset the DC components and provide suitable amplification prior to digitizing the signals with a 12-bit A/D converter (RC electronics) on a personal computer (NEC 386). A sampling frequency  $f_s$  equal to  $2 f_c$  was used in all cases and the record duration was 50 s. The digital data were directly transferred from the personal computer to a VAX 8550 computer using an ETHERNET (fibre optic cable) link. The spatial and temporal derivatives and their squared values were formed on the VAX computer.

TABLE I. Moments of temperature derivatives.

		Round jet (present)		Planet jet (Antonia et al.)	Isotropic value 
$x_2/R_u$	0.0	0.53	1.07	0	
$x_2/R_u$ $K_{21}^2$ $K_{31}^2$ $K_{21}^4$ $K_{31}^4$	0.98	1.04	1.15	2	1
$K_{31}^{2}$	1.03	1.08	1.2	•••	1
$K_{21}^{4}$	1.03	0.83	0.6	0.4	1
$K_{31}^{4}$	0.95	0.85	0.62	•••	1
$S_{\theta_1}$	-1.1	-1.08	-1.15	-0.85	0
$S_{\theta_2}$	-0.05	-0.86	-1.01	≈0	0
$S_{\theta_2}^{1}$ $S_{\theta_3}$	-0.04	0.1	-0.08	•••	0

#### III. DEPARTURE FROM LOCAL ISOTROPY

Local isotropy of the scalar field requires that

$$p(\theta_{.1}) = p(\theta_{.2}) = p(\theta_{.3})$$

and

$$p(-\theta_{i})=p(\theta_{i}).$$

One consequence of this is the equality

$$\langle \theta_{.1}^n \rangle = \langle \theta_{.2}^n \rangle = \langle \theta_{.3}^n \rangle. \tag{2}$$

When *n* is odd,  $\langle \theta_{,i}^n \rangle = 0$  (in particular, the skewness  $S_{\theta_{,i}} \equiv \langle \theta_{,i}^3 \rangle / \langle \theta_{,i}^2 \rangle^{3/2} = 0$ ); when *n* is even, the following ratios:

$$K_{21}^{n} = \frac{\langle \theta_{,2}^{n} \rangle}{\langle \theta_{,1}^{n} \rangle}$$

and

$$K_{31}^n = \frac{\langle \theta_{,3}^n \rangle}{\langle \theta_{,1}^n \rangle}$$

are unity. These ratios for n=2 and 4 and the magnitudes of  $S_{\theta,i}$  (i=1,2,3) are presented in Table I for  $x_2/R_u=0$ , 0.53, and 1.07. As noted in Sec. II, the present data were estimated from the finite difference  $\theta_i \sim \Delta \theta/\Delta x_i$  at the optimum separation  $\Delta x_i \approx 3\eta$ . Also shown in the table are the corresponding values obtained by Antonia et al. 28 in the self-preserving region ( $x_1/d=40$ ) of a slightly heated turbulent plane jet. Table I indicates that the isotropic requirement (2) for n=2 is very closely satisfied on the axis. It is less adequately satisfied as  $x_2$  increases. Away from the axis, the departure from (2) is more pronounced at n=4 than n=2. The departure of  $K_{21}^n$  from unity is considerably larger for the plane jet, even on the centerline. This implies that local isotropy of the scalar field is more closely satisfied in the round jet than in the plane jet, as previously noted in Ref. 13.

The nonzero values of the skewnesses  $S_{\theta,i}$  for i=1 and 2 (off the axis), which seem to invalidate the assumption of local isotropy, are associated with the mean temperature gradient  $\langle T \rangle_{,i}$  (e.g., Refs. 29–31). The nonzero value of  $S_{\theta,i}$  may not mainly reflect the anisotropy of the small-scale temperature field.  $^{28,32,33}$  It is more likely associated with the asymmetry of the large-scale motion. Figure 1 shows the cospectrum,  $\mathrm{Co}_{\theta,i}\theta_{,i}^2$ , between  $\theta_{,i}$  and  $\theta_{,i}^2$  for i=1 and 2 at  $x_2/R_u=0$  and 0.53. The cospectrum is normalized such that the area under the curve is equal to  $|S_{\theta,i}|$ . The major contri-

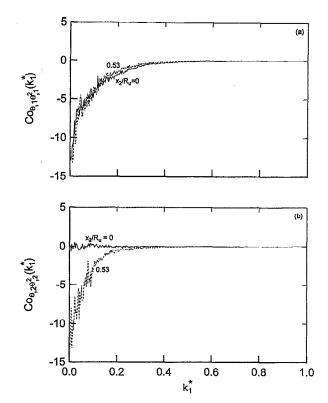


FIG. 1. Cospectra between  $\theta_{,i}$  and  $\theta_{,i}^2$  (i=1,2) at  $x_2/R_u=0$  (---) and 0.53 (---). (a) i=1; (b) 2.

bution (>65%) to  $S_{\theta_{1}}$  or  $S_{\theta_{2}}$  at  $x_{2}/R_{u}=0.53$  occurs in the range  $k_1^* \le 0.1$ , suggesting that the nonzero values of  $S_{\theta}$ result mainly from the asymmetry of the large-scale motion. As a result of symmetry with respect to  $x_2$ , the cospectrum  $\operatorname{Co}_{\theta_2\theta_2^2}$  is nearly zero at all values of  $k_1^*$  [Fig. 1(b)] on the jet axis. However, when  $k_1^* \leq 0.2$ ,  $\operatorname{Co}_{\theta_1,\theta_1^2}$  is negative both on and off the axis since the large scale streamwise motion is asymmetrical with respect to  $x_1$  across the jet (as reflected by the presence of ramps in the temperature signals). Sreenivasan et al.<sup>32</sup> provided more direct evidence of the influence of the large-scale motion on the magnitude of  $S_{\theta_1}$  in a round jet. A conditional technique was used for removing the effect of the large-scale motion on  $\theta$ , the skewness of the  $x_1$  derivative of the remaining signal was nearly zero. It is possible that  $S_{\theta,1}$  is not a reliable indicator of local isotropy. The magnitude of  $S_{\theta_1}$  is virtually unchanged ( $\approx 1.1$ ) at different  $x_2/R_\mu$  (Table I); Sreenivasan et al.<sup>32</sup> noted that the magnitude of  $|S_{\theta_1}|$  ( $\approx$ 0.8) did not change either for different flows or over several orders-of-magnitude variation in  $R_{\lambda}$ .

#### IV. CORRELATION BETWEEN $\theta$ AND $\epsilon_{\theta}$

The JPDF of  $\theta_{,t}^2$  and  $\theta_{,i}^2$  (i=1,2, or 3) is shown in Fig. 2. Clearly, there are important differences between  $\theta_{,1}^2$  and either  $\theta_{,2}^2$  or  $\theta_{,3}^2$ . Figure 2(a) implies a relatively high degree of correlation between  $\theta_{,t}^2$  and  $\theta_{,1}^2$ . The correlation coefficient, i.e.,  $\langle \theta_{,t}^{2*} \theta_{,1}^{2*} \rangle$  [hereafter, the asterisk denotes a variable which is centered and normalized by the root-mean-square (RMS) value], between these two variables is greater than

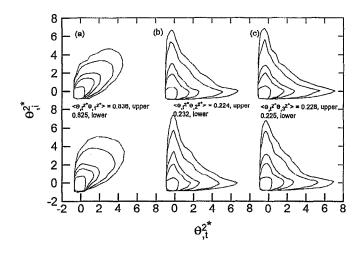


FIG. 2. Normalized JPDF contours of  $\theta_{,t}^2$  and  $\theta_{,t}^2$ . (a)  $p(\theta_{,t}^{2*}, \theta_{,1}^{2*})$ ; (b)  $p(\theta_{,t}^{2*}, \theta_{,2}^{2*})$ ; (c)  $p(\theta_{,t}^{2*}, \theta_{,3}^{2*})$ . Outer to inner contours: 0.0005, 0.001, 0.005, 0.01, and 0.1. Upper and lower contours are for  $x_2/R_u = 0$  and 0.53.

0.8 at all  $x_2$  locations. This coefficient should be 1 if Taylor's hypothesis, i.e.,  $\theta_{,t} = -\langle U_1 \rangle$   $\theta_{,1}$ , applies. Figures 2(b) and 2(c) show a close coincidence between large values of  $\theta_{,t}^{2*}$  and small values of  $\theta_{,2}^{2*}$  and  $\theta_{,3}^{2*}$  and vice versa, indirectly suggesting that periods of strong activity in  $\theta_{,2}^{2*}$  and  $\theta_{,3}^{2*}$  may occur almost simultaneously and correspond to periods where  $\theta_{,1}^{2*}$  is quiescent. An important consequence of this is that the instantaneous behavior of  $\epsilon_{\theta}$  cannot be inferred solely on the basis of  $\theta_{,1}^{2}$ . This should be kept in mind, especially when only the  $\theta_{,1}^{2}$  data are available.

Estimates of the correlation coefficient between  $\theta$  and fluctuations of  $\theta_{,i}^2$  have been made both for  $\theta < 0$  and  $\theta > 0$ . A zero value of the coefficient in each case can result from either of the following conditions: (i) statistical independence between  $\theta$  and  $\theta_{,i}^2$ , (ii)  $p(\theta^*, +\theta_{,i}^{2^*}) = p(\theta^*, -\theta_{,i}^{2^*})$ , viz. symmetry of  $p(\theta_{,i}^{2^*})$ . In the present flow, condition (ii) is not satisfied since the skewness of  $\theta_{,i}^{2^*}$  is in the range 10-20, i.e.,  $p(\theta_{,i}^{2^*})$  is far from being symmetrical. A zero value of the correlation coefficient, when  $\theta$  is either positive or negative, would therefore be consistent with the notion of independence between  $\theta$  and  $\theta_{,i}^2$ . Note that a zero value of the correlation does not necessarily imply independence, e.g., Figure 6.9 of Tennekes and Lumley; strictly, Eq. (1) needs to be verified. Table II indicates that, at  $x_2/R_u \le 0.8$ , the correlation coefficient is very

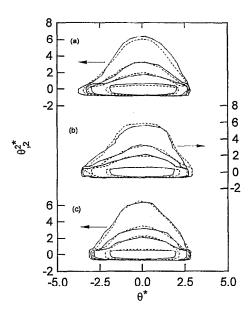


FIG. 3. Independence check for the JPDF of  $\theta$  and  $\theta_2^2$ . (a)  $x_2/R_u=0$ ; (b) 0.53; (c) 0.8. —,  $p(\theta^*, \theta_2^{1^*})$ ; —,  $p(\theta^*)p(\theta_{,2}^{1^*})$ . Outer to inner contours: 0.0005, 0.002, 0.006, and 0.05.

small, typically less than 0.05, for both  $\theta$ <0 and  $\theta$ >0. This implies that there is a very weak dependence between  $\theta$  and  $\theta_{,i}^2$ . Since  $\epsilon_{\theta} \equiv \alpha(\theta_{,1}^2 + \theta_{,2}^2 + \theta_{,3}^2)$ , the dependence between  $\epsilon_{\theta}$  and  $\theta$  is expected to be also very weak; as shown in Table II, the magnitude of the normalized correlation

$$\frac{\langle \theta \epsilon_{\theta} \rangle}{\langle \theta^{2} \rangle^{1/2} \langle \epsilon_{\theta} \rangle} = \frac{\langle \theta \theta_{,1}^{2} \rangle + \langle \theta \theta_{,2}^{2} \rangle + \langle \theta \theta_{,3}^{2} \rangle}{\langle \theta^{2} \rangle^{1/2} \langle \langle \theta_{,1}^{2} \rangle + \langle \theta_{,2}^{2} \rangle + \langle \theta_{,3}^{2} \rangle)},\tag{3}$$

is indeed quite close to zero at all measurement locations. This, in turn, suggests that Eq. (1) is approximately valid; direct checks of the relation  $p(\theta^*, \theta_{,2}^{2^*}) = p(\theta^*)p(\theta_{,2}^{2^*})$  (Fig. 3) corroborate this.

Figure 4 indicates that the correlation coefficients  $\langle \theta^* \theta_{,i}^{2^*} \rangle$  increase slightly with  $x_2/R_u$ , as noted in Ref. 15 in the context of a plane jet. In both jets,  $S_\theta$  varies in a manner similar to  $\langle \theta^* \theta_{,i}^{2^*} \rangle$ , where the data of  $S_\theta$  for the plane jet  $(x_1/d=40)$  were taken from Ref. 35. Note, however, that in the range  $x_2/R_u \leq 1$  or  $x_2/L_u \leq 1$  ( $L_u$  is the plane jet halfwidth), both  $S_\theta$  and  $\langle \theta^* \theta_{,i}^{2^*} \rangle$  are significantly closer to zero for the round jet than for the plane jet. Accordingly, one could conclude, as did Anselmet *et al.*, <sup>16</sup> that the correlation between  $\theta$  and  $\theta_{i}^2$  [or  $\epsilon_\theta$ ] is, to a large degree, related to the

TABLE II. Correlation coefficients between  $\theta$  and the temperature dissipation components. The normalized correlation between  $\theta$  and  $\epsilon_{\theta}$  is also shown.

$x_2/R_u$	$\langle heta^* heta_{,1}^{2*} angle$		$\langle  heta^* heta_{,2}^{2*} angle$		$\langle heta^* heta_{,3}^{2*} angle$		
	θ*<0	<i>θ</i> >0	<i>θ</i> *<0	<i>θ</i> *>0	<i>θ</i> *<0	<i>θ</i> *>0	$\langle   heta^* \epsilon_{ heta}  angle / \langle \epsilon_{ heta}  angle$
0	-0.06	0.017	-0.065	0.016	-0.061	0.012	-0.086
0.27	-0.066	0.022	-0.032	0.003	-0.036	0.004	0.063
0.53	-0.038	0.033	-0.032	0.009	-0.054	-0.001	-0.047
0.80	-0.017	0.032	-0.018	0.009	-0.032	0.01	-0.028
1.07	0.059	0.086	-0.018	0.043	-0.047	0.049	0.038

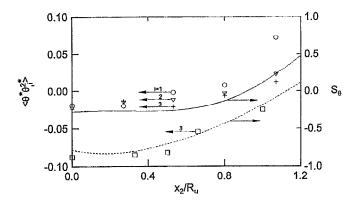


FIG. 4. Distributions of  $\langle \theta^* \theta_{,i}^{2^*} \rangle$  and  $S_{\theta}$ . Round jet (present):  $\bigcirc$ ,  $\langle \theta^* \theta_{,1}^{2^*} \rangle$ ;  $\triangle$ ,  $\langle \theta^* \theta_{,2}^{2^*} \rangle$ ; +,  $\langle \theta^* \theta_{,3}^{2^*} \rangle$ ; --,  $S_{\theta}$ . Plane jet:  $\square$ ,  $\langle \theta^* \theta_{,3}^{2^*} \rangle$  (Anselmet and Antonia<sup>15</sup>); --,  $S_{\theta}$  (Browne *et al.*<sup>35</sup>).

magnitude of  $S_{\theta}$ . It is unlikely, however, that  $S_{\theta}$  is the only factor, since the location where  $S_{\theta}$  is zero does not coincide with that where  $\langle \theta^* \theta_{,i}^{2^*} \rangle$  is zero [also see Fig. 4(b) of Ref. 16]. Figure 3 suggests that Eq. (1) is as closely validated on the axis  $[S_{\theta} \sim -0.3]$  and the departure of  $p(\theta)$  from symmetry is not negligible] as at  $x_2/R_u = 0.8$  ( $S_\theta$  is negligible there). Yet, the data presented in Table I indicate that local isotropy is more closely satisfied on the axis. Similarly, the lack of correlation between  $\theta$  and  $\theta_{,i}^2$  (i=1,2) obtained by Namazian et al., 11 on the axis in the developing region  $(x_1/d \le 17)$  of a round jet, should be associated with a non-negligible value of  $S_{\theta}$ , on the basis of the data shown in Ref. 19 in the region  $2.5 \le x_1/d \le 30$  of a round jet. Perhaps more importantly, the data of Refs. 11 and 12 support the isotropy of  $\langle \epsilon_{\theta} \rangle$ , at least approximately, on the jet axis. In a slightly heated round jet, Anselmet et al. 16 also obtained a very small value (≈0.05) of  $\langle \theta^* \theta_{.1}^{2^*} \rangle$  at  $x_1/d=15$  and  $x_2=0$ , where  $S_{\theta} \approx -0.5$ . Moreover, consistently with the relative magnitudes of  $\langle \theta^* \theta_i^{2*} \rangle$  in Fig. 4, the departure from local isotropy is significantly smaller in the round jet than in the plane jet (Sec. III). These results are not unreasonable if one interprets local isotropy as reflecting a lack of dependence between the small-scale motion (which contributes significantly to  $\langle \epsilon_{\theta} \rangle$  and the large-scale motion (which dominates the magnitude of  $\langle \theta^2 \rangle$ ). The above discussion strongly supports that the correlation  $\langle \theta \epsilon_{\theta} \rangle$  is influenced not just by the symmetry of  $p(\theta)$  but also by the level of departure from local isotropy.

Jayesh and Warhaft<sup>36</sup> presented estimates of the correlation coefficient  $\rho = \langle \theta^{2*} \epsilon_{\theta}^* \rangle$  and the normalized correlation  $\rho_P = (\langle \theta^2 \epsilon_{\theta} \rangle / \langle \epsilon_{\theta} \rangle - 1)$  for decaying grid turbulence with and without a mean lateral temperature gradient  $\langle T \rangle_2$ . In their case,  $\epsilon_{\theta}$  was inferred from  $\theta_t^2$ , via Taylor's hypothesis. With an imposed constant  $\langle T \rangle_2$ ,  $\rho$  and  $\rho_P$  were typically 0.1 and 0.4 at the last measurement station, suggesting a significant correlation between the scalar and its dissipation rate  $\epsilon_{\theta}$ . At this station,  $p(\theta)$  is quite symmetrical (we estimated a value of 0.03 for  $S_{\theta}$ ). In the same flow, Tong and Warhaft<sup>37</sup> showed that, when  $\langle T \rangle_2 \neq 0$ , the departure of  $\langle \epsilon_{\theta} \rangle$  from isotropy is significant (typically  $K_{21}^2 = 1.52 \pm 0.2$ ). This is ex-

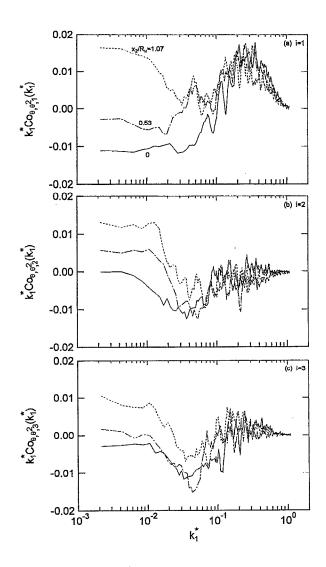


FIG. 5. Cospectra of  $\theta$  and  $\theta_i^2$  at three values of  $x_2/R_u$ . (a) i=1; (b) 2; (c) 3; ---,  $x_2/R_u=0$ ; ---, 0.53; ..., 1.07.

pected since an imposed mean temperature gradient can act as a source of temperature anisotropy in grid turbulence. When  $\langle T \rangle_2 \approx 0$ ,  $\rho$  and  $\rho_P$  were significantly reduced to about 0.03 and 0.1, respectively. Yet, a discernible departure from symmetry can be detected in  $p(\theta)$  (see their Fig. 16), the value of  $S_{\theta}$  being approximately 0.2. One would expect  $\epsilon_{\theta}$  to satisfy isotropy roughly in this case. Note that, for the present experiments,  $\rho$  and  $\rho_P$  are less than 0.01 on the axis, implying a much smaller degree of correlation between the scalar and its dissipation rate than for decaying grid turbulence.

#### V. STATISTICAL DEPENDENCE BETWEEN heta AND $\epsilon_{ heta}$

In order to gain further insight into the dependence between  $\theta$  and  $\theta_{,i}^2$ , cospectra of  $\theta$  and  $\theta_{,i}^2$  are shown in Fig. 5, in the form  $k_1^* \operatorname{Co}_{\theta,\theta_{,i}^2}$  vs  $\log_{10} k_1^*$  (where  $k_1^* = k_1 \eta$ ), at three radial locations  $(x_2/R_u=0, 0.53, \text{ and } 1.07)$ . Relatively large magnitudes occur in the range  $0 < k_1^* \le 0.1$ , reflecting the importance of the large-scale motion. For  $k_1^* > 0.1$ , the

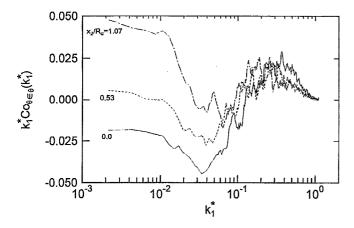


FIG. 6. Cospectra of  $\theta$  and  $\epsilon_{\theta}$  at three values of  $x_2/R_u$ . —,  $x_2/R_u=0$ ; ---, 0.53; ..., 1.07.

magnitude of  $\operatorname{Co}_{\theta,\theta_{,1}^2}$  remains discernible (typically less than 0.015), while  $\operatorname{Co}_{\theta,\theta_{,2}^2}$  and  $\operatorname{Co}_{\theta,\theta_{,3}^2}$  are almost zero at all wave numbers. This indicates that the statistical dependence between  $\theta$  and  $\theta_{,i}^2$  is weak for i=2 and 3 but relatively strong for i=1. Although  $\theta_{,i}^2$  for i=1, 2, and 3 were not obtained simultaneously, the cospectrum between  $\theta$  and  $\epsilon_{\theta}$ , i.e.,  $\operatorname{Co}_{\theta,\epsilon_{\theta}}$ , can be estimated approximately using the data for  $\operatorname{Co}_{\theta,\epsilon_{\theta}}$ . Figure 6 shows data for  $\operatorname{Co}_{\theta,\epsilon_{\theta}}(k_1^*)$ ; note that

$$\frac{\langle \theta \epsilon_{\theta} \rangle}{\langle \theta^2 \rangle^{1/2} \langle \epsilon_{\theta} \rangle} = \int \operatorname{Co}_{\theta, \epsilon_{\theta}}(k_1^*) dk_1^*.$$

As  $x_2$  increases, the main variation in the cospectrum occurs at  $k_1^* \lesssim 0.1$ :  $\operatorname{Co}_{\theta,\epsilon_{\theta}}(k_1^*)$ , which is negative on the axis, becomes positive when  $x_2/R_u \gtrsim 0.5$ . This suggests that, on average, low temperatures ( $\theta < 0$ ), which are associated with the entrained partially-mixed (cooler) fluid, would be related to relatively high dissipation rates  $\epsilon_{\theta}$  (greater than  $\langle \epsilon_{\theta} \rangle$ ) in the central flow region.

Further evidence of the dependence between  $\theta_{,i}^2$  and  $\theta$  can be obtained from measurements of  $\langle \theta_{,i}^2 | \theta \rangle$ , the expectation of  $\theta_{,i}^2$  conditioned on individual values of  $\theta$ . This expectation is defined (e.g., Ref. 21) as follows:

$$\langle \theta_{,i}^{2} | \theta \rangle = \int_{-\infty}^{\infty} \theta_{,i}^{2} p(\theta_{,i} | \theta) d\theta_{,i}, \qquad (4)$$

where

$$p(\theta_{,i}|\theta) = \frac{p(\theta,\theta_{,i})}{p(\theta)}$$

is the conditional PDF of  $\theta_{,i}$  (i=1,2,3) for particular values of  $\theta$ . Estimates of  $\langle \theta_{,i}^2 | \theta \rangle$  were made at  $x_2/R_u$ =0, 0.53, and 1.07; the normalized distributions of  $q_i(\theta) \equiv \langle \theta_{,i}^2 | \theta \rangle / \langle \theta_{,i}^2 \rangle$  are shown in Fig. 7. For all values of i,  $q_i(\theta)$  exhibit a peak (not well-defined) near both the lower and upper limits of the temperature range. High-temperature dissipation rates can occur at the interface—where there is a high-temperature difference and therefore strong mixing—between the large-scale warmer fluid and the entrained cooler fluid; this interface is reflected by a relatively large jump in the temperature signal.

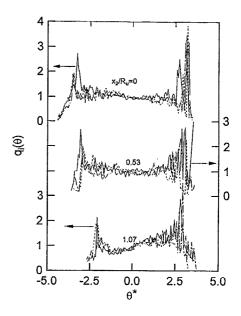


FIG. 7. Distributions of  $q_i(\theta)$  at  $x_2/R_{\mu}=0$ , 0.53, and 1.07. —, i=1; ---, 2; ..., 3.

Since the cooler entrained fluid comes in contact with warmer fluid at the interface, high values of  $\theta_{i}^{2}$  may be associated with either low or high values of  $\theta^*$ , thus leading to the two observed peaks of  $q_i(\theta)$ . The largest values of  $|\theta|$  are associated with the smallest values of  $q_i(\theta)$ . This is reasonable since temperatures associated with the coolest unmixed or partially mixed fluid and the warmest well-mixed (fully turbulent) fluid are unlikely to be dissipated rapidly. Further, note that, at  $x_2/R_u=0$  and 0.53, the left peak in  $q_1(\theta)$  is stronger than that in either  $q_2(\theta)$  or  $q_3(\theta)$ , the latter two being nearly equal. The right peak appears to be of equal strength for all i, although the jitter and likely lack of convergence of the data make conclusions difficult. A possible explanation is that the interface in the central flow region may, on average, be approximately normal to the  $x_1$  direction, so that a relatively large streamwise temperature change occurs. When conditioning is on the spatially coherent temperature jump, a very sharp increase is observed in  $\langle \theta_{.1}^2/\theta \rangle$  (see Fig. 9 of Ref. 13) near the jump location, where  $\theta$  is generally negative and thus associated with the cooler entrained fluid. Increases in both  $\theta_{,2}^2$  and  $\theta_{,3}^2$  also occur at almost the same location but their magnitude is smaller than that of  $\theta_1^2$ . The jitter and poor convergence of  $\langle \theta^2_i / \theta \rangle$  near the high-temperature side requires comment. While much longer record durations would reduce the fluctuations, it is unlikely that they would yield a better definition of  $q_i(\theta)$ . Kailasnath et al.<sup>38</sup> found that, even for very long record durations (~15 h) obtained in the wake of a heated cylinder,  $q_1(\theta)$  did not converge at the uppermost temperature end (unpublished wake data obtained in our laboratory corroborate this). The authors suggested that this lack of convergence reflects the infrequent arrival at the measurement station of very high-temperature fluid (in the present case the upper temperature limit would correspond to the temperature at the jet exit).

For  $|\theta^*| \lesssim 2$ ,  $q_i(\theta) \approx 1$  at  $x_2/R_u = 0$  and 0.53. This indicates negligible statistical dependence between  $\theta$  and  $\theta^2$ , for

 $|\theta^*| \leq 2$ . For statistical independence between  $\theta$  and  $\theta_{i}^2$  $\langle \theta_{,i}^2 | \theta \rangle = \langle \theta_{,i}^2 \rangle$  or  $q_i(\theta) = \langle \theta_{,i}^2 | \theta \rangle / \langle \theta_{,i}^2 \rangle = 1$ . The probability that  $\theta^*$  falls in the range  $|\theta^*| > 2$  is quite small ( $\leq 5\%$ ). This negates the effects of the extrema of  $q_i(\theta)$  at large  $|\theta^*|$  so that  $\langle \theta^* \theta_{i}^{2*} \rangle$  is nearly zero when  $x_2/R_u \lesssim 0.5$  (Sec. IV). At  $x_2/R_n = 1.07$ , except near the two limits of  $\theta^*$ ,  $q_i(\theta)$  increases noticeably as  $\theta^*$  increases. At this location, the departure from local isotropy is more significant than on the axis (Sec. III). Consistent with this, Southerland and Dahm<sup>14</sup> observed that, in a round water jet at  $x_1/d\approx 235$  and  $x_2/x_1=0.11$ , the conditional dissipation rate  $\langle \epsilon_{\theta} | \theta \rangle$  is generally an increasing function of  $\theta$  (in this case,  $\theta$  should be identified with the dye concentration fluctuation). These authors found a nonnegligible departure from local isotropy (e.g.,  $K_{21}^2 \approx 1.1$  and  $K_{31}^2 \approx 1.5$ ) at the same off-axis location (unfortunately, no information was given on the axis).

In decaying grid-generated turbulence, the statistical behavior of  $q(\theta) \equiv \langle \epsilon_{\theta} | \theta \rangle / \langle \epsilon_{\theta} \rangle$ , inferred from Taylor's hypothesis, was investigated by Jayesh and Warhaft<sup>36</sup> at  $\langle T \rangle_{,2} = C$  (a nonzero constant) and  $\langle T \rangle_2 = 0$ . When  $\langle T \rangle_2 = C$ ,  $q(\theta)$  depends strongly on  $\theta$  and exhibits a rounded V shape (symmetrical about  $\theta=0$ ) at all measurement stations  $x_1/M$ ( $\leq$ 160), where M is the grid mesh length. In this case, as mentioned in Sec. IV, the departure of  $\langle \epsilon_{\theta} \rangle$  from isotropy is significant.<sup>37</sup> When  $\langle T \rangle_{,2} \approx 0$ , the distribution of  $q(\theta)$  shows a strong peak near the upper limit of  $\theta$  at  $x_1/M = 62.4$  but becomes much flatter, especially for  $\theta^* \leq 0$  where  $q(\theta) \approx 1$ , at  $x_1/M = 82.4$ . Although these authors were not able to measure  $q(\theta)$  at further downstream distances, the trend suggests that  $q(\theta)$  tends to unity, i.e.,  $\langle \epsilon_{\theta} \rangle$  tends to be statistically independent of  $\theta$ , as  $x_1$  increases. We believe that  $\langle \epsilon_{\theta} \rangle$  should tend to isotropy in this case. Another interesting difference in  $q(\theta)$  for the two cases is that, when  $\langle T \rangle_2 \approx 0$ , like the present results for the round jet, the largest temperature fluctuations, either positive or negative, are associated with the lowest values of  $\epsilon_{\theta}$ ; when  $\langle T \rangle_{.2} = C$ , however, the largest fluctuations are related to the highest dissipation rates.

The significant difference between the present behavior of  $q_i(\theta)$  and that obtained by Kailasnath et al.<sup>38</sup> on the axis of a round water jet at  $x_1/d=37$  ( $R_d=3900$ ) requires comment. On the axis, their distributions of  $q_i(\theta)$  (i=1 or 2) increases very significantly with  $\theta$  (see Fig. 5 of Ref. 38). The rate of increase is several times larger than for the present  $q_i(\theta)$  at  $x_2/R_u=1.07$  and Southerland and Dahm's <sup>14</sup>  $q_i(\theta)$  at  $x_2/R_u \approx 1$ . Since  $\langle \theta^* \theta_{,i}^{2^*} \rangle = \langle \theta^* \langle \theta_{,i}^{2^*} | \theta^* \rangle \rangle$ , the  $q_i(\theta)$  distributions of Kailasnath *et al.* suggest that  $\langle \theta^* \theta_i^{2^*} \rangle$ should differ significantly from zero, in contrast to the present nearly zero value (Fig. 4). Also, their absolute values of  $S_A$  should be considerably larger than the present value of  $|S_{\theta}|$ . The present value of  $S_{\theta}$  ( $\approx -0.3$ ) on the axis is comparable to that obtained by Birch et al. 17 in a C<sub>3</sub>H<sub>8</sub> air round jet  $(S_{\theta} = -0.3)$  and Pitts and Kashiwagi<sup>18</sup> in a CH<sub>4</sub> air round jet  $(S_{\theta} \approx -0.4)$ . The present value is also not very different from that (~-0.5) obtained by Anselmet et al. 16 on the axis at  $x_1/d=15$ . However, in the same jet as used in Ref. 38, Prasad and Sreenivasan<sup>39</sup> obtained a much bigger value (>1) for  $S_{\theta}$  in the region  $13 \le x_1/d \le 21$ . The observed differences between the present data and those of Ref. 38 may be attrib-

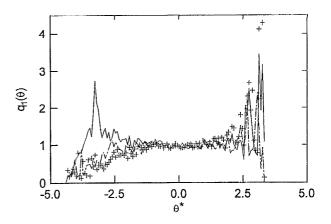


FIG. 8. Comparison between  $q_1(\theta)$  and  $q_1'(\theta)$  at  $x_2/R_u=0$ . —,  $q_1(\theta)$ ; ---,  $q_1'(\theta)$  for  $\theta=\frac{1}{2}(\theta_1+\theta_{i-1})$ ; +,  $q_1'(\theta)$  for  $\theta=\theta_j$ .

uted to significant differences in initial conditions between the two flows. This seems plausible as Gao and O'Brien<sup>40</sup> found, using direct numerical simulations of isotropic turbulence, that a nonzero correlation between  $\theta$  and  $\theta_{,i}$  is primarily the result of initial conditions. Similarly, in decaying grid-generated turbulence, Jayesh and Warhaft<sup>36</sup> noted that the residual effect of initial conditions, although not evident in  $\langle T \rangle$  and  $\langle \theta^2 \rangle$ , affects  $p(\theta)$  and  $q(\theta)$  significantly, even at large distances downstream. While the above observations apply to homogeneous turbulence, similar results could be expected for inhomogeneous turbulent shear flows. The effect of initial conditions clearly merits further study.

## VI. EFFECT OF TAYLOR'S HYPOTHESIS ON $Q_1(\theta)$

To investigate the effect of using Taylor's hypothesis on the measurement of  $q_1(\theta) = \langle \theta_1^2/\theta \rangle / \langle \theta_1^2 \rangle$ , a comparison is made, in Fig. 8, between the directly measured  $q_1(\theta)$  and  $q_1^t(\theta)$ , inferred from Taylor's hypothesis. The distribution of  $q_1^t(\theta)$  is only single-lobed near the high-temperature side; as found by Kailasnath et al. 38 Like  $q_1(\theta)$ ,  $q_1^t(\theta)$  is quite flat over the range  $|\theta^*| \le 2$ . However, this plateau is absent in Kailasnath et al.'s distribution for  $q_1^t(\theta)$ , the latter increasing monotonically with  $\theta$ . A possible reason for this is that there may be differences in the initial conditions between the two jets. Another possibility is as follows. Let  $\{\theta_i\}$  (j=1,2,...)represent the discrete time series of  $\theta$ . An approximation for  $(\theta_{,t})_j$  is given by  $(\theta_j - \theta_{j-1})/\tau_s$ , where  $\tau_s = f_s^{-1}$ . If  $(\theta_{,t})_j$  is the instantaneous derivative at the instant when  $\theta_i$  occurs, one would expect that  $q_1^t(\theta)$  will weight larger values of  $\theta$ more heavily, since the temperature signal often exhibits ramp-like patterns (a jump followed by a gradual decrease; see Ref. 32). This expectation is corroborated by Fig. 8 and is consistent with the distribution of  $q_1^t(\theta)$  obtained by Ref. 38 [we are assuming that they estimated  $q_1^t(\theta)$  in this way]. It is worth pointing out that the finite difference  $(\theta_i - \theta_{i-1})/\tau_s$ is an adequate approximation to the time derivative when  $\theta = (\theta_i + \theta_{i-1})/2$  but not for  $\theta = \theta_i$ , since the zero value of  $\langle \theta \theta_{t} \rangle [\equiv \frac{1}{2} (\langle \theta^2 \rangle)_{t}]$ , which follows from the stationarity of  $\theta$ , is obtained only when  $\theta = (\theta_i + \theta_{i-1})/2$ .

The comparison in Fig. 8 indicates that, on the axis, Taylor's hypothesis is approximately valid for estimating  $q_1(\theta)$  when  $\theta^* \ge -2$  but inadequate when  $\theta^* \le -2$ . This should not introduce any significant error to the conventional average  $\langle \theta_{,1}^2 \rangle$ , since the magnitude of  $\int_{-\infty}^{-2} p(\theta^*) d\theta^*$  is quite small. 25,41 The breakdown for  $\theta^* \le -2$  is readily explained; the magnitude of  $\theta_{,t}$  at a point in space depends on how rapidly  $\theta$  changes with time; this change should be closely related to the instantaneous velocity of the fluid at temperature  $(\langle T \rangle + \theta)$ . Obviously, the coolest (entrained) fluid should have a streamwise velocity which is much smaller than the local mean streamwise velocity  $\langle U_1 \rangle$ . Therefore, the use of Taylor's hypothesis, i.e.,  $\theta_{,t} = -\langle U_1 \rangle \theta_{,1}$ , will cause a significant attenuation of  $\langle \theta_{,t}^2 | \theta \rangle \langle U_1 \rangle^{-2}$  near the low temperature side; as a result, the low temperature peak in  $q_1(\theta)$  is not evident in  $q_1^t(\theta)$  (Fig. 6). Recent results obtained by Tong and Warhaft<sup>42</sup> in a round jet corroborate this. It is difficult to understand why Kailasnath et al.'s distributions of  $q_1^t$  and  $q_1$ are identical on the low concentration side.

#### VII. CONCLUSIONS

The dependence between  $\theta$  and  $\epsilon_{\theta}$  is influenced not only by the symmetry of  $p(\theta)$ , as was pointed out by Anselmet  $et\ al.$ , <sup>16</sup> but also by the departure from local isotropy. The dependence is weaker in a round jet than a plane jet, the difference reflecting the smaller departure from local isotropy for the round jet. The expectation of  $\epsilon_{\theta}$ , conditioned on  $\theta$ , depends strongly on  $\theta$  when the latter is either very positive or negative. This local dependence is due to the close connection which exists between the large-scale motion and the entrainment of unmixed or partially mixed fluid; this connection does not however contribute significantly to the correlation  $\langle \theta \epsilon_{\theta} \rangle$ .

In the fully turbulent part of the flow the conditional expectation  $\langle \theta_i^2/\theta \rangle$  is independent of i when  $-2 \leq \theta^* \leq 2$ . Within this range, the magnitude of the expectation is nearly 1, implying approximate independence between  $\theta_i^2$  or  $\epsilon_{\theta}$  and  $\theta$ . For  $\theta^* \leq -2$ , there are significant differences in  $\langle \theta_i^2/\theta \rangle$  between i=1 and i=2 (or 3). Contrary to the conclusion of Kailasnath et al.,  $^{38}$  our data indicate that estimates of  $\langle \theta_i^2/\theta \rangle$  from  $\langle \theta_i^2/\theta \rangle$  and Taylor's hypothesis are seriously in error near the low-temperature side. On the high-temperature side  $(\theta^* \geq 2)$ , it is possible that differences exist in  $\langle \theta_i^2/\theta \rangle$  for different i. In this region, the poor convergence of the data which, as noted in Ref. 38, is mainly due to the infrequent arrivals of high-temperature fluid, makes it difficult to draw any conclusions.

## **ACKNOWLEDGMENT**

The support of the Australian Research Council is gratefully acknowledged.

- <sup>1</sup>R. W. Bilger, "Turbulent diffusion flames," Annu. Rev. Fluid Mech. 21, 101 (1989).
- <sup>2</sup>R. W. Bilger, "Turbulent mixing and reaction," Proceedings of the Eleventh Australasian Fluid Mechanics Conference, Hobart, pp. 1–9, 1992.
- <sup>3</sup>K. M. C. Bray, "Turbulent flows with premixed reactants," in *Topics in Applied Physics: Turbulent Reacting Flows*, edited by P. A. Libby and F. A. Williams (Springer-Verlag, Berlin, 1980), Vol. 44, pp. 115–183.
- <sup>4</sup>R. W. Bilger, "Turbulent flows with non-premixed reactants," in *Topics in*

- Applied Physics: Turbulent Reacting Flows, edited by P. A. Libby and F. A. Williams (Springer-Verlag, Berlin, 1980), Vol. 44, pp. 63-113.
- <sup>5</sup>T. T. Yeh and C. W. Van Atta, "Spectral transfer of scalar and velocity fields in heated grid turbulence," J. Fluid Mech. 58, 233 (1973).
  <sup>6</sup>Z. Warhaft and J. L. Lumley, "An experimental study of the decay of
- <sup>6</sup>Z. Warhaft and J. L. Lumley, "An experimental study of the decay of temperature fluctuations in grid-generated turbulence," J. Fluid Mech. 88, 659 (1978).
- <sup>7</sup>S. Tavoularis and S. Corrsin, "Experiments in nearly homogeneous turbulent shear flow with a uniform mean temperature gradient, Part 1," J. Fluid Mech. **104**, 311 (1981).
- <sup>8</sup>R. A. Antonia and L. W. B. Browne, "The destruction of temperature fluctuations in a turbulent plane jet," J. Fluid Mech. 134, 67 (1983).
- <sup>9</sup>R. A. Antonia and L. W. B. Browne, "Anisotropy of the temperature dissipation in a turbulent wake," J. Fluid Mech. 163, 393 (1986).
- <sup>10</sup>L. V. Krishnamoorthy and R. A. Antonia, "Temperature dissipation measurements in a turbulent boundary layer," J. Fluid Mech. 176, 265 (1987).
- <sup>11</sup>M. Namazian, R. W. Schefer, and J. Kelly, "Scalar dissipation measurements in the developing region of a jet," Combust. Flame 74, 147 (1988).
- <sup>12</sup>R. W. Schefer, A. R. Kerstein, M. Namazian, and J. Kelly, "Role of large-scale structure in a nonreacting turbulent CH<sub>4</sub> jet," Phys. Fluids 6, 652 (1994).
- <sup>13</sup>R. A. Antonia and J. Mi, "Temperature dissipation in a turbulent round jet," J. Fluid Mech. 250, 531 (1993).
- <sup>14</sup>K. B. Southerland and W. J. A. Dahm, "A four-dimensional experimental study of conserved scalar mixing in turbulent flows," Report No. 026779-12, The University of Michigan, 1994.
- <sup>15</sup>F. Anselmet and R. A. Antonia, "Joint statistics between temperature and its dissipation in a turbulent jet," Phys. Fluids 28, 1048 (1985).
- <sup>16</sup>F. Anselmet, H. Djeridi, and L. Fulachier, "Joint statistics between a passive scalar and its dissipation in turbulent flows," J. Fluid Mech. 280, 173 (1994).
- <sup>17</sup>A. D. Birch, D. Brown, M. G. Dodson, and J. R. Thomas, "The turbulent concentration field of a methane jet," J. Fluid Mech. 88, 431 (1978).
- <sup>18</sup>W. M. Pitts and T. Kashiwagi, "The application of laser-induced Rayleigh light scattering to the study ρf<sub>i</sub> turbulent mixing," J. Fluid Mech. **141**, 391 (1984).
- <sup>19</sup>L. P. Chua and R. A. Antonia, "The turbulent interaction region of a circular jet," Int. Commun. Heat Mass Transfer 13, 545 (1986).
- <sup>20</sup>E. E. O'Brien, "Turbulent flows with non-premixed reactants," in *Topics in Applied Physics: Turbulent Reacting Flows*, edited by P. A. Libby and F. A. Williams (Springer-Verlag, Berlin, 1980), Vol. 44, pp. 185–218.
- <sup>21</sup>S. B. Pope, "PDF Methods for turbulent reactive flows," Progr. Energy Combust. Sci. 11, 119 (1985).
- <sup>22</sup>R. W. Bilger, "Conditional moment closure for turbulent reacting flow," Phys. Fluids A 5, 436 (1993).
- <sup>23</sup>W. E. Mell, V. Nilsen, G. Kosaly, and J. J. Riley, "Investigation of closure models for nonpremixed turbulent reacting flows," Combust. Sci. Tech. 91, 179 (1994).
- <sup>24</sup>R. A. Antonia and J. Mi, "Corrections for velocity and temperature derivatives in turbulent flows," Exp. Fluids 14, 203 (1993).
- <sup>25</sup>J. Mi and R. A. Antonia, "Some checks of Taylor's hypothesis in a slightly heated turbulent circular jet," Exp. Therm. Fluid Sci. 8, 328 (1994).
- <sup>26</sup>P. Paranthoen, C. Petit, and J. C. Lecordier, "The effect of thermal prongwire interaction on the response of cold wire in gaseous flows (air, argon and helium)," J. Fluid Mech. 124, 457 (1982).
- <sup>27</sup>J. C. Wyngaard, "Spatial resolution of a resistance wire temperature sensor," Phys. Fluids 14, 2052 (1971).
- <sup>28</sup>R. A. Antonia, F. Anselmet, and A. J. Chambers, "Assessment of local isotropy using measurements in a turbulent plane jet," J. Fluid Mech. 192, 211 (1986).
- <sup>29</sup>C. H. Gibson, C. A. Friehe, and O. McConnell, "Structure of sheared turbulent fields," Phys. Fluids Suppl. 20, S156 (1977).
- <sup>30</sup>K. R. Sreenivasan and S. Tavoularis, "On the skewness of the temperature derivative in turbulent flows," J. Fluid Mech. 101, 783 (1980).
- <sup>31</sup>R. Budwig, S. Tavoularis, and S. Corrsin, "Temperature fluctuations and heat flux in grid-generated isotropic turbulence with streamwise and transverse mean temperature gradients," J. Fluid Mech. 153, 441 (1985).
- <sup>32</sup> K. R. Sreenivasan, R. A. Antonia, and D. Britz, "Local isotropy and large structures in a heated turbulent jet," J. Fluid Mech. 94, 745 (1979).
- <sup>33</sup>R. A. Antonia and C. W. Van Atta, "Structure functions of temperature fluctuations in turbulent shear flows," J. Fluid Mech. 84, 561 (1978).
- <sup>34</sup>H. Tennekes and J. L. Lumley, A First Course in Turbulence (MIT Press, Cambridge, MA, 1972).
- <sup>35</sup>L. W. B. Browne, R. A. Antonia, and A. J. Chambers, "The interaction

region of a turbulent plane jet," J. Fluid Mech. 149, 355 (1984).

- <sup>36</sup> Jayesh and Z. Warhaft, "Probability distribution, conditional dissipation and transport of passive temperature fluctuations in grid-generated turbulence," Phys. Fluids A 4, 2292 (1992).
- <sup>37</sup>C. Tong and Z. Warhaft, "On passive scalar derivative statistics in grid turbulence," Phys. Fluids 6, 2165 (1994).
- <sup>38</sup>P. Kailasnath, K. R. Sreenivasan, and J. R. Saylor, "Conditional scalar dissipation rates in turbulent wakes, jets, and boundary layers," Phys. Fluids A 5, 3207 (1993).
- <sup>39</sup>R. R. Prasad and K. R. Sreenivasan, "Quantitative three-dimensional imaging and the structure of passive scalar fields in fully turbulent flows," J. Fluid Mech. 216, 1 (1990).
- <sup>40</sup>F. Gao and E. E. O'Brien, "Joint probability density function of a scalar and its gradient in isotropic turbulence," Phys. Fluids A 3, 1625 (1991).
- <sup>41</sup>J. Mi and R. A. Antonia, "Corrections to Taylor's hypothesis in a turbulent circular jet," Phys. Fluids 6, 1548 (1994).
- <sup>42</sup>C. Tong and Z. Warhaft, "Passive scalar dispersion and mixing in a turbulent jet," to appear in J. Fluid Mech. (1995).