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APPENDIX A

SELECTED CONE PENETRATION TEST RESULTS FROM FIELD STUDY

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Figure A.1 Cone penetration test results from sounding A0.



Figure A.2 Cone penetration test results from sounding A1.



Figure A.3 Cone penetration test results from sounding A2.



Figure A.4 Cone penetration test results from sounding A4.



Figure A.5 Cone penetration test results from sounding A6.



Figure A.6 Cone penetration test results from sounding A8.



Figure A.7 Cone penetration test results from sounding A10.



Figure A.8 Cone penetration test results from sounding B1.



Figure A.9 Cone penetration test results from sounding B5.



Figure A.10 Cone penetration test results from sounding B8.



Figure A.11 Cone penetration test results from sounding C0.



Figure A.12 Cone penetration test results from sounding C4.



Figure A.13 Cone penetration test results from sounding C8.

	The University of Adelaide Cone Penetration Test								
Client: Department of Civil and Environmental Engineering									
Job Details: PhD Research									
Test	cetion: C8								
Surface R.L.: 40.911 m AHD Date: 24th July, 1992 Time: 1:33 pm									
	Cone Tin	Sleeve	Friction	I	Cone Tin	Sleeve	Friction		
Depth	Boeletanco	Eriction	Ratio	Depth	Besistance	Eriction	Batio		
(m)		Filction ((m)	nesistance	f (kDa)			
	q _c (MPa)	<u>ц</u> (кна)	F _R (70)			1, (KFa)	Γ _R (70)		
0.005	0.22	N/A	N/A	0.215	1.14	77.20	6.77		
0.010	N/A	19.10	N/A	0.220	1.09	78.20	7.17		
0.015	0.48	N/A	N/A	0.225	1.07	74.30	6.94		
0.020	N/A	20.00	N/A	0.230	1.06	78.20	7.38		
0.025	0.60	21.00	3.50	0.235	1.07	82.10	7.67		
0.030	0.67	24.40	3.64	0.240	1.09	80.60	7.39		
0.035	0.67	26.90	4.01	0.245	1.06	77.20	7.28		
0.040	0.65	28.80	4.43	0.250	1.07	76.20	7.12		
0.045	0.79	32.30	4.09	0.255	1.03	78.20	7.59		
0.050	0.89	35.70	4.01	0.260	1.00	77.70	7.77		
0.055	N/A	37.10	N/A	0.265	1.09	77.20	7.08		
0.060	1.00	37.10	3.71	0.270	1.04	78.20	7.52		
0.065	N/A	40.10	N/A	0.275	1.14	78.20	6.86		
0.070	0.88	42.00	4.77	0.280	1.09	85.50	7.84		
0.075	1.03	43.50	4.22	0.285	1.14	79.70	6.99		
0.080	N/A	45.90	N/A	0.290	1.09	81.60	7.49		
0.085	1.06	48.90	4.61	0.295	1.11	77.20	6.95		
0.090	N/A	51.80	N/A	0.300	1.11	79.70	7.18		
0.095	1.03	50.80	4.93	0.305	1.03	77.70	7.54		
0.100	1.03	53.30	5.17	0.310	1.11	73.30	6.60		
0.105	1.06	53.30	5.03	0.315	0.95	73.30	7.72		
0.110	1.09	56.70	5.20	0.320	0.97	75.30	7.76		
0.115	1.06	57.70	5.44	0.325	0.98	71.40	7.29		
0.120	1.07	58.20	5.44	0.330	1.06	71.80	6.77		
0.125	1.11	60.10	5.41	0.335	1.06	69.40	6.55		
0.130	1.14	61.10	5.36	0.340	1.03	72.30	7.02		
0.135	1.09	60.60	5.56	0.345	1.09	71.80	6.59		
0.140	1.11	65.00	5.86	0.350	1.11	67.40	6.07		
0.145	1.13	59.60	5.27	0.355	1.17	70.90	6.06		
0.150	1.11	63.50	5.72	0.360	1.20	70.40	5.87		
0.155	1.13	68.90	6.10	0.365	1.16	70.40	6.07		
0.160	1.16	68.40	5.90	0.370	1.19	70.40	5.92		
0.165	1.13	65.00	5.75	0.375	1.23	69.40	5.64		
0.170	1.07	68.40	6.39	0.380	1.29	69.40	5.38		
0.175	1.11	68.40	6.16	0.385	1.32	62.10	4.70		
0.180	1.10	71.40	6.49	0.390	1.38	62.60	4.54		
0.185	1.13	73.30	6.49	0.395	1.26	60.10	4.77		
0.190	1.14	70.40	6.18	0.400	1.33	N/A	N/A		
0.195	1.13	72.30	6.40	0.405	1.36	59.60	4.38		
0.200	1.11	/6.20	6.86	0.410	1.51	64.50	4.27		
0.205	1.11	/4.80	6.74	0.415	1.52	58.70	3.86		
0.210	1.11	/5.30	ნ./ბ	0.420	1.4/	01.10	4.10		

Figure A.14 Cone penetration test data from sounding C8 (1 of 13).

The University of Adelaide Cone Penetration Test									
Client: Department of Civil and Environmental Engineering									
Job Details: PhD Research									
Test Location: C8									
Surface R.L.: 40.911 m AHD Date: 24th July. 1992 Time: 1:33 pm									
 									
Depth	Cone Tip	Sleeve	Friction	Depth	Cone Tip	Sleeve	Friction		
(m)	Resistance	Friction	Ratio	(m)	Resistance	Friction	Ratio		
	q _c (MPa)	ť, (kPa)	F _R (%)		q _c (MPa)	f, (kPa)	F _R (%)		
0.425	1.60	64.50	4.03	0.635	1.35	55.70	4.13		
0.430	1.61	61.10	3.80	0.640	1.33	61.10	4.59		
0.435	1.69	63.50	3.76	0.645	1.35	56.20	4.16		
0.440	1.66	66.00	3.98	0.650	1.32	58.20	4.41		
0.445	1.51	63.50	4.21	0.655	1.30	54.30	4.18		
0.450	1.54	66.00	4.29	0.660	1.38	59.10	4.28		
0.455	1.54	63.50	4.12	0.665	1.23	60.10	4.89		
0.460	1.50	67.40	4.49	0.670	1.23	63.50	5.16		
0.465	1.60	68.40	4.28	0.675	1.30	59.60	4.58		
0.470	1.58	68.40	4.33	0.680	1.25	59.10	4.73		
0.475	N/A	67.40	N/A	0.685	1.14	56.70	4.97		
0.480	1.60	67.40	4.21	0.690	1.17	56.20	4.80		
0.485	1.72	64.00	3.72	0.695	1.19	51.80	4.35		
0.490	1.73	65.00	3.76	0.700	1.20	51.80	4.32		
0.495	1.77	69.40	3.92	0.705	1.14	54.70	4.80		
0.500	1.73	66.50	3.84	0.710	1.25	53.80	4.30		
0.505	1.80	67.90	3.77	0.715	1.22	54.70	4.48		
0.510	1.85	67.90	3.67	0.720	1.23	53.80	4.37		
0.515	1.88	68.40	3.64	0.725	1.19	52.80	4.44		
0.520	1.92	63.50	3.31	0.730	1.14	57.20	5.02		
0.525	1.98	69.40	3.51	0.735	1.14	50.30	4.41		
0.530	1.91	66.00	3.46	0.740	1.17	55.20	4.72		
0.535	1.91	55.00	3.46	0.745	1.13	54.30	4.81		
0.540	1.66	70.90	3.77	0.750	1.28	54.30	4.24		
0.545	1.00	72 20	3./5	0.755	1.20	57.20	4.77		
0.555	1.00	70.00	0.80 A 10	0.700	1.19	57.20	4.81		
0.560	164	67.00	4.14	0.700	1.20	52.50	4.19		
0.565	164	69.40	4.03 A 92	0.775	1.20	57.20	4.81		
0.570	1.70	68.40	4.02	0.775	1.30	57.20	4.40		
0.575	1.54	64.50	4 19	0.785	1.55	80.10	4.01		
0.580	1.60	62.10	3,88	0.790	1 17	59.60	4.90		
0.585	1.60	61.60	3.85	0.795	1.30	58.20	0.0 0		
0.590	1.51	62.60	4.15	0.800	1.22	57 70	4 73		
0.595	1.42	63.50	4,47	0.805	1.20	59.10	403		
0.600	1.44	62.10	4.31	0.810	1.20	63.50	5.29		
0.605	1.50	62.10	4.14	0.815	1.29	64.50	5,00		
0.610	1.48	63.00	4.26	0.820	1.23	66.50	5.41		
0.615	1.33	58.20	4.38	0.825	1.17	66.00	5.64		
0.620	1.30	57.20	4.40	0.830	1.19	66.50	5.59		
0.625	1.29	59.10	4.58	0.835	1.11	65.50	5.90		
0.630	1.28	56.70	4.43	0.840	1.20	60.60	5.05		

Figure A.15 Cone penetration test data from sounding C8 (2 of 13).

	The University of Adelaide Cone Penetration Test					Page 3 of 13			
Client: Department of Civil and Environmental Engineering									
Job Details: PhD Research									
Test Lo	ocation: C8								
Surface R.L.: 40.911 m AHD Date: 24th July, 1992 Time: 1:33 pm									
	Cone Tip	Sleeve	Friction		Cone Tip	Sleeve	Friction		
Depth	Resistance	Friction	Ratio	Depth	Resistance	Friction	Ratio		
(m)	q. (MPa)	f, (kPa)	F ₂ (%)	(m)	q. (MPa)	f, (kPa)	F. (%)		
		,							
0.845	1.11	64.00	5.77	1.055	1.63	70.40	4.32		
0.850	1.16	67.40	5.81	1.060	1.58	70.40	4.46		
0.855	1.23	65.50	5.33	1.065	1.54	72.80	4.73		
0.860	1.11	62.10	5.59	1.070	1.5/	//.20	4.92		
0.865	1.23	62.60	5.09	1.075	1.01	82.60	5.13		
0.875	1.20	64.00	5.09	1.000	1.72	105.60	6.56		
0.875	1.20	69.90	5.20	1.000	1.01	133.00	8.32		
0.885	1.19	74.30	5.07	1.050	1.01	N/A	N/A		
0.000	1.20	73.80	6.31	1 100	1.66	132.90	8.01		
0.895	1.28	73.30	5 73	1 105	1.00	N/A	N/A		
0.000	1 29	68.90	5.34	1 110	1.69	133.90	792		
0.905	1.20	70.90	5.50	1 115	1.00	112.90	6.64		
0.910	1.28	72.80	5.69	1.120	1.70	N/A	N/A		
0.915	1.26	70.90	5.63	1 125	1.77	80.60	4.55		
0.920	1.29	69.40	5.38	1.130	1.74	100.70	5.79		
0.925	1.33	68.90	5.18	1.135	1.76	102.60	5.83		
0.930	1.26	72.30	5.74	1.140	1.73	106.50	6.16		
0.935	1.33	75.30	5.66	1.145	1.82	110.50	6.07		
0.940	1.23	73.30	5.96	1.150	1.83	116.30	6.36		
0.945	1.22	70.90	5.81	1.155	1.85	117.30	6.34		
0.950	1.25	73.80	5.90	1.160	1.92	122.70	6.39		
0.955	1.25	72.80	5.82	1.165	2.20	135.40	6.15		
0.960	1.23	70.40	5.72	1.170	N/A	174.00	N/A		
0.965	1.26	72.30	5.74	1.175	2.23	178.40	8.00		
0.970	1.23	70.40	5.72	1.180	N/A	175.00	N/A		
0.975	1.35	71.40	5.29	1.185	2.20	171.10	7.78		
0.980	1.23	71.80	5.84	1.190	2.14	165.70	7.74		
0.985	1.19	72.30	6.08	1.195	N/A	162.30	N/A		
0.990	1.25	72.80	5.82	1.200	1.72	159.30	9.26		
0.995	1.33	71.40	5.37	1.205	1.85	153.00	8.27		
1.000	1.29	76.20	5.91	1.210	1.83	151.00	8.25		
1.005	1.26	76.70	6.09	1.215	1.80	148.60	8.26		
1.010	1.25	72.30	5.78	1.220	1.80	145.70	8.09		
1.015	1.29	71.80	5.57	1.225	1.80	138.80	7.71		
1.020	1.35	72.30	5.36	1.230	1.77	N/A	N/A		
1.025	1.48	75.80	5.12	1.235	1.69	132.90	7.86		
1.030	1.45	71.40	4.92	1.240	1.74	132.00	7.59		
1.035	1.54	71.40	4.64	1.245	1.82	120.70	6.63		
1.040	1.58	69.40	4.39	1.250	1.82	118.30	6.50		
1.045	1.64	69.40	4.23	1.255	1.86	118.30	6.36		
1.050	1.66	68.90	4.15	1.260	1.88	115.30	6.13		

Figure A.16 Cone penetration test data from sounding C8 (3 of 13).
		The C	Univers one Pene	ity of A Stration	delaide Test	Page 4	of 13
	Client: Dep	artment of Civ	vil and Enviror	nmental En	gineering		-
Job	Details: PhD	Research					
Toet L	cotion: Ca						
Test Lu			-				
Surfa	ce R.L.: 40.9	11 m AHD	Date	: 24th July	, 1992	Time: 1	1:33 pm
	Cone Tin Sleeve Eriction Cone Tin Sle						Eriction
Depth	Resistance	Eriction	Patio	Depth	Pacietanco	Eriction	Potio
(m)	(MDo)	f (kDe)		(m)	nesistance	(///Do)	
	q _c (MiPa)	ц (кра)	F _R (%)		q, (MPa)	т, (кра)	F _R (%)
1.265	1.86	115.80	6.23	1.475	2.02	163.20	8.08
1.270	1.88	116.80	6.21	1.480	2.02	165.20	8.18
1.275	1.83	110.00	6.01	1.485	2.08	N/A	N/A
1.280	1.83	113.90	6.22	1.490	2.04	N/A	N/A
1.285	1.83	114.40	6.25	1.495	2.11	192.60	9.13
1.290	1.83	112.90	6.17	1.500	2.16	188.70	8.74
1.295	1.89	114.90	6.08	1.505	2.11	187.20	8.87
1.300	1.91	113.90	5. 9 6	1.510	2.07	188.70	9.12
1.305	N/A	121.70	N/A	1.515	2.04	185.70	9.10
1.310	2.02	121.20	6.00	1.520	2.08	188.70	9.07
1.315	2.05	122.70	5.99	1.525	1.96	188.70	9.63
1.320	2.02	129.00	6.39	1.530	2.07	192.60	9.30
1.325	1.92	128.10	6.67	1.535	2.05	189.60	9.25
1.330	1.91	135.90	7.12	1.540	1.94	187.20	9.65
1.335	2.01	134.90	6.71	1.545	1.91	191.60	10.03
1.340	1.96	141.30	7.21	1.550	1.95	191.60	9.83
1.345	1.96	N/A	N/A	1.555	1.91	188.70	9.88
1.350	2.07	142.20	6.87	1.560	N/A	187.70	N/A
1.355	2.08	147.10	7.07	1.565	N/A	189.60	N/A
1.360	2.09	153.00	7.01	1.570	1.00	189.00	10.09
1.305	2.00	156.40	7.40	1.575	1.91	195.20	9.00
1.375	1 99	157.40	7.45	1.500	1.94	185.20	9.55
1 380	2 01	163.20	8.12	1.505	1.95	183.30	9.52
1.385	1 99	156.90	7.88	1.595	1.94	180.40	9.45
1.390	2.04	161.30	7,91	1,600	2.01	177 40	8.83
1.395	1.96	163.20	8.33	1,605	1.99	179.40	9.02
1.400	1.92	163.20	8.50	1.610	2.02	175.50	8.69
1.405	1.94	166.20	8.57	1.615	2.07	173.00	8,36
1.410	1.96	168.10	8.58	1.620	2.07	167.60	8.10
1.415	1.92	165.20	8.60	1.625	2.08	167.20	8.04
1.420	N/A	170.10	N/A	1.630	2.14	167.60	7.83
1.425	1.98	163.20	8.24	1.635	2.08	168.60	8.11
1.430	1.94	168.60	8.69	1.640	2.04	168.10	8.24
1.435	1.89	162.30	8.59	1.645	2.14	173.00	8.08
1.440	1.96	165.20	8.43	1.650	2.11	174.50	8.27
1.445	1.96	163.20	8.33	1.655	2.08	174.00	8.37
1.450	1.94	165.20	8.52	1.660	2.02	171.10	8.47
1.455	1.91	165.70	8.68	1.665	2.01	177.40	8.83
1.460	2.02	163.20	8.08	1.670	2.02	175.50	8.69
1.465	2.02	160.30	7.94	1.675	2.04	175.00	8.58
1.470	1.95	160.80	8.25	1.680	2.11	180.40	8.55

Figure A.17 Cone penetration test data from sounding C8 (4 of 13).

	The University of Adelaide Cone Penetration Test Page 5 of 13 Page 5 of 13										
	Client: Depa	artment of Civ	ril and Environ	imental En	gineering						
Job	Details: PhD	Research									
Test	cation: C8										
Surfa	ce R.L.: 40.91	11 m AHD	Date	: 24th July	, 1992	Time: 1	:33 pm				
	Cone Tin	Cone Tin Sleeve Eriction Cone Tin					Friction				
Depth	Boeietanca	Eriction	Batio	Depth	Resistance	Friction	Batio				
(m)		f (kBa)	E (%)	(m)	a (MPa)	f (kPa)	E (%)				
		((KPA)	F _R (70)	-		4 (NF 0)	·R (/d)				
1.685	2.01	179.90	8.95	1.895	1.64	131.00	7.99				
1.690	2.01	178.40	8.88	1.900	1.66	132.00	7.95				
1.695	2.11	177.40	8.41	1.905	1.74	126.60	7.28				
1.700	2.14	178.40	8.34	1.910	1.69	131.50	7.78				
1.705	2.17	183.80	8.47	1.915	1.74	124.60	7.16				
1.710	2.08	186.70	8.98	1.920	1.79	128.10	7.16				
1.715	2.11	191.10	9.06	1.925	1.74	127.60	7.33				
1.720	2.14	189.60	8.86	1.930	1.76	129.00	7.33				
1.725	2.07	193.10	9.33	1.935	1.79	130.00	7.26				
1.730	2.11	192.60	9.13	1.940	1.72	127.10	7.39				
1.735	2.16	191.10	8.85	1.945	1.80	136.90	7.61				
1.740	2.16	190.10	8.80	1.950	1.74	132.50	7.61				
1.745	2.04	192.60	9.44	1.955	1.//	138.80	7.84				
1.750	2.08	196.50	9.45	1.960	1.72	141.30	8.22				
1.755	2.13	195.00	9.15	1.965	1.79	141.70	7.92				
1.760	2.14	196.00	9.16	1.970	1.63	138.80	8.52				
1.765	2.05	N/A	N/A	1.975	1.74	147.10	0.40				
1.770	2.02	197.50	9.78	1.980	1.72	143.20	0.33				
1.//5	1.94	193.50	9.97	1.965	1.03	145.20	0.91				
1.780	1.92	190.60	9.93	1.990	1.60	139.80	8.95				
1.765	1.00	185.00	10.09	2 000	1.55	142 20	9.17				
1.790	1.03	184.20	10.00	2.000	1.55	144.20	9.13				
1.795	1.73	183.30	10.65	2.005	1.50	141.30	9.00				
1.000	1.00	180.80	10.10	2.010	1.57	142.20	9.06				
1.810	1.75	179.90	10.64	2.020	1.57	139.30	9.23				
1.010	1.63	173.00	10.55	2.025	1.51	141.70	9.38				
1 820	1.66	171.10	10.31	2.030	1.48	140.30	9.48				
1 825	1.61	164.70	10.23	2,035	1.52	142.20	9.36				
1.830	1.57	161.30	10.27	2.040	1.51	134.40	8.90				
1.835	1.54	160.30	10.41	2.045	1.42	139.80	9.85				
1 840	N/A	159.30	N/A	2.050	1.47	137.30	9.34				
1.845	1.51	150.00	9.93	2.055	1.54	133.90	8.69				
1.850	1.57	145.70	9.28	2.060	1.51	136.90	9.07				
1.855	1.51	141.30	9.36	2.065	1.51	130.00	8.61				
1.860	1.48	141.30	9.55	2.070	1.48	130.50	8.82				
1.865	1.48	135.90	9.18	2.075	1.47	126.60	8.61				
1.870	1.47	135.90	9.24	2.080	1.41	126.10	8.94				
1.875	1.54	134.90	8.76	2.085	1.36	125.10	9.20				
1.880	1.54	136.40	8.86	2.090	1.39	128.50	9.24				
1.885	1.60	134.90	8.43	2.095	1.47	131.00	8.91				
1.890	1.60	134.90	8.43	2.100	1.35	129.50	9.59				

Figure A.18 Cone penetration test data from sounding C8 (5 of 13).



2.220

2.225

2.230

2.235

2.240

2.245

2.250

2.255

2.260

2.265

2.270

2.275

2.280

2.285

2.290

2.295

2.300

2.305

2.310

1.36

1.28

1.35

1.29

1.32

1.39

1.32

1.38

1.29

1.26

1.29

1.29

1.25

1.30

1.26

1.32

1.41

1.35

1.38

132.00

126.10

130.00

128.50

127.10

132.90

133.40

130.00

130.00

125.60

124.60

128.50

126.60

129.50

132.00

132.90

128.10

131.00

131.50

9.71

9.85

9.63

9.96

9.63

9.56

10.11

9.42

10.08

9.97

9.66

9.96

10.13

10.48

10.07

9.09

9.70

9.53

9.96

2.430

2.435

2.440

2.445

2.450

2.455

2.460

2.465

2.470

2.475

2.480

2.485

2.490

2.495

2.500

2.505

2.510

2.515

2.520

1.28

1.25

1.38

1.35

1.35

1.35

1.48

1.45

1.42

1.45

1.42

1.36

1.35

1.39

1.38

1.42

1.32

1.38

1.36

118.80

123.20

118.80

123.70

121.70

120.70

126.60

125.60

125.60

126.60

128.50

124.60

125.60

127.60

123.70

126.60

122.20

127.10

121.70

9.28

9.86

8.61

9.16

9.01

8.94

8.55

8.66

8.85

8.73

9.05

9.16

9.30

9.18

8.96

8.92

9.26

9.21

8.95

The University of Adelaide

	Cone Penetration Test Page 6 of 13											
	Client: Dep	partment of Ci	ivil and Enviro	nmental E	ngineering	• • • • • • • • • • • • • • • • • • • •						
Job	Details: PhD	Research										
Test L	ocation: C8											
Surfa	ice R.L.: 40.9	11 m AHD	Date	: 24th July	<i>ı</i> , 1992	Time:	1:33 pm					
Depth (m)	Cone Tip Resistance q _e (MPa)	Sleeve Friction t, (kPa)	Friction Ratio F _R (%)	Depth (m)	Cone Tip Resistance q. (MPa)	Sleeve Friction f, (kPa)	Friction Ratio F _R (%)					
2.105	1.39	132.90	9.56	2.315	1.35	129.00	9.56					
2.110	1.41	133.90	9.50	2.320	1.38	132.90	9.63					
2.115	1.35	133.40	9.88	2.325	1.32	127.60	9.67					
2.120	1.32	134.90	10.22	2.330	1.35	130.00	9.63					
2.125	1.36	134.90	9.92	2.335	1.38	130.00	9.42					
2.130	1.29	135.90	10.53	2.340	1.38	128.50	9.31					
2.135	1.35	135.40	10.03	2.345	1.45	132.50	9.14					
2.140	1.30	132.90	10.22	2.350	1.33	128.10	9.63					
2.145	1.36	134.90	9.92	2.355	1.35	126.10	9.34					
2.150	1.30	131.00	10.08	2.360	1.42	127.10	8.95					
2.155	1.30	132.90	10.22	2.365	1.33	120.70	9.08					
2.160	1.32	129.00	9.77	2.370	1.35	121.20	8.98					
2.165	1.38	127.10	9.21	2.375	1.33	120.70	9.08					
2.170	1.38	126.10	9.14	2.380	1.39	117.80	8.47					
2.175	1.35	125.10	9.27	2.385	1.39	117.80	8.47					
2.180	1.39	125.10	9.00	2.390	1.42	119.30	8.40					
2.185	1.41	122.70	8.70	2.395	1.39	117.80	8.47					
2.190	1.35	125.10	9.27	2.400	1.35	116.80	8.65					
2.195	1.29	124.60	9.66	2.405	1.32	118.80	9.00					
2.200	1.42	124.60	8.77	2.410	1.29	117.30	9.09					
2.205	1.42	124.60	8.77	2.415	1.22	118.30	9.70					
2.210	1.39	127.60	9.18	2.420	1.36	118.80	8.74					
2.215	1.32	128.10	9.70	2.425	1.26	119.70	9.50					
			-	-			-					

Figure A.19 Cone penetration test data from sounding C8 (6 of 13).

	The University of Adelaide Cone Penetration Test Page 7 of 13 Page 7 of 13											
	Client: Depa	artment of Civ	il and Enviror	nmental En	gineering							
Job	Details: PhD	Research										
Teet	acetion: C8											
Surfa	ce B.I.: 40.9	11 m AHD	Date	: 24th July	1992	Time: 1	:33 pm					
- Ouna	1		1		1		T					
Donth	Cone Tip	Sleeve	Friction	Depth	Cone Tip	Sleeve	Friction					
Depth	Resistance	Friction	Ratio	Deptil	Resistance	Friction	Ratio					
(m)	q _c (MPa)	f, (kPa)	F _R (%)	(m)	q _c (MPa)	f _s (kPa)	F _R (%)					
2.525	1.35	121.20	8.98	2.735	1.52	130.00	8.55					
2.530	1.38	119.30	8.64	2.740	1.48	126.10	8.52					
2.535	1.35	121.20	8.98	2.745	1.45	128.10	8.83					
2.540	1.29	120.70	9.36	2.750	1.54	127.10	8.25					
2.545	1.29	121.20	9.40	2.755	1.45	127.60	8.80					
2.550	1.35	121.70	9.01	2.760	1.50	129.50	8.63					
2.555	1.35	118.80	8.80	2.765	1.51	130.00	8.61					
2.560	1.32	119.30	9.04	2.770	1.52	131.00	8.62					
2.565	1.28	114.40	8.94	2.775	1.60	132.90	8.31					
2.570	1.38	117.80	8.54	2.780	1.51	132.00	8.74					
2.575	1.30	117.80	9.06	2.785	N/A	134.40	N/A					
2.580	1.30	114.90	8.84	2.790	1.55	129.00	8.32					
2.585	1.39	120.70	8.68	2.795	1.52	129.00	8.49					
2.590	1.44	117.80	8.18	2.800	1.45	131.50	9.07					
2.595	1.35	119.70	8.87	2.805	1.45	128.10	8.83					
2.600	1.42	117.80	8.30	2.810	1.48	125.10	8.45					
2.605	1.39	122.70	8.83	2.815	1.42	125.10	8.81					
2.610	1.39	120.70	8.68	2.820	1.48	123.70	8.36					
2.615	1.51	123.70	8.19	2.825	1.47	126.10	8.58					
2.620	1.35	126.10	9.34	2.830	1.47	127.60	8.68					
2.625	1.47	125.60	8.54	2.835	1.38	127.10	9.21					
2.630	1.42	124.60	8.77	2.840	1.39	120.70	8.68					
2.635	1.44	129.50	8.99	2.845	1.41	122.70	8.70					
2.640	1.41	127.60	9.05	2.850	1.41	125.10	8.87					
2.645	1.50	130.50	8.70	2.855	1.39	124.60	8.96					
2.650	1.52	128.10	8.43	2.860	1.32	120.20	9.11					
2.655	1.47	131.00	8.91	2.865	1.39	122.70	8.83					
2.660	1.50	130.50	8.70	2.870	1.32	119.70	9.07					
2.665	1.41	134.90	9.57	2.875	1.29	125.10	9.70					
2.670	1.48	130.00	8.78	2.880	1.38	119.30	8.64					
2.675	1.42	133.40	9.39	2.885	1.41	116.30	8.25					
2.680	1.35	134.90	9.99	2.890	1.30	117.30	9.02					
2.685	1.42	137.80	9.70	2.895	1.38	117.80	8.54					
2.690	1.39	135.90	9.78	2.900	1.42	113.90	8.02					
2.695	1.39	139.80	10.06	2.905	1.35	113.40	8.40					
2.700	1.47	132.90	9.04	2.910	1.42	111.90	7.88					
2.705	1.41	136.90	9.71	2.915	1.29	114.90	8.91					
2.710	1.38	N/A	N/A	2.920	1.38	112.90	8.18					
2.715	1.39	134.90	9.71	2.925	1.29	110.00	8.53					
2.720	1.44	132.90	9.23	2.930	1.38	110.00	7.97					
2.725	1.48	132.90	8.98	2.935	1.35	103.60	7.67					
2.730	1.47	126.10	8.58	2.940	1.32	110.50	8.37					

Figure A.20 Cone penetration test data from sounding C8 (7 of 13).

	The University of Adelaide Cone Penetration Test										
	Client: Depa	artment of Civ	il and Enviror	nmental En	gineering						
Job	Details: PhD	Research									
Test Lo	ocation: C8										
Surfa	ce R.L.: 4 0.91	1 m AHD	Date	: 24th July	, 1992	Time: 1	l :33 pm				
	Cone Tin	Sleeve Friction Cone Tip Sle					Friction				
Depth	Boeietance	Eriction	Ratio	Depth	Resistance	Friction	Betio				
(m)		f (kBa)	E (%)	(m)		f (kBa)	E (%)				
	q _c (mra)	i, (KFa)	F _R (76)			i, (KPA)	r _R (70)				
2.945	1.38	109.00	7.90	3.155	1.38	103.10	7.47				
2.950	1.32	108.50	8.22	3.160	1.38	104.10	7.54				
2.955	1.23	111.40	9.06	3.165	1.44	103.10	7.16				
2.960	1.29	109.50	8.49	3.170	1.57	106.50	6.78				
2.965	1.32	111.90	8.48	3.175	1.54	104.10	6.76				
2.970	1.32	112.40	8.52	3.180	1.51	106.10	7.03				
2.975	1.32	112.90	8.55	3.185	1.48	103.60	7.00				
2.980	1.28	110.90	8.66	3.190	1.48	105.60	7.14				
2.985	1.26	109.00	8.65	3.195	1.51	107.00	7.09				
2.990	1.30	108.50	8.35	3.200	1.54	103.60	6.73				
2.995	1.35	111.40	8.25	3.205	1.54	104.60	6.79				
3.000	1.26	110.50	8.77	3.210	1.51	107.00	7.09				
3.005	1.35	112.90	8.36	3.215	1.54	106.50	6.92				
3.010	1.32	111.90	8.48	3.220	1.51	105.60	6.99				
3.015	1.30	112.40	8.65	3.225	1.52	103.60	6.82				
3.020	1.32	113.40	8.59	3.230	1.42	105.10	7.40				
3.025	1.38	109.00	7.90	3.235	1.51	106.10	7.03				
3.030	1.35	115.30	8.54	3.240	1.54	104.10	6.76				
3.035	1.29	115.80	8.98	3.245	1.48	105.60	7.14				
3.040	1.23	114.90	9.34	3.250	1.58	106.10	6.72				
3.045	1.30	119.70	9.21	3.255	1.51	107.00	7.09				
3.050	1.30	115.30	8.87	3.260	1.60	110.90	6.93				
3.055	1.22	117.80	9.66	3.265	1.54	108.50	1.05				
3.060	1.28	118.30	9.24	3.2/0	1.5/	110.50	0.91				
3.000	1.20	115.60	9.20	3.2/5	1.00	110.90	7.10				
3.070	1.20	120.70	9.43 0.50	3.200	1.04	112.00	7.30				
3.0/5	1.20	119.70	9.50	3.200	1.57	115.90	6.00				
3.080	1.23	146.00	9.09 0.50	3.290	1.00	115.60	0.90				
3.000	1.23	116 90	9.00 0.07	3 200	1.00	116 20	0.90				
3.005	1.20	112.00	9.27 0.41	3 205	1.00	118 80	7.50				
3 100	1.20	114 40	9,30	3 310	1.60	119 70	7.91				
3 105	1.20	112 00	9.00	3,315	1.60	120 70	7.54				
3 110	1 32	112.50	8.52	3,320	1.66	127 10	7.66				
3.115	1.33	113.40	8.53	3.325	1.69	125.10	7.40				
3.120	1.38	110.50	8.01	3,330	1.64	125.60	7.66				
3,125	1.35	110.90	8.21	3.335	1.70	127.10	7.48				
3.130	1.45	110.00	7.59	3.340	1.72	128.50	7.47				
3.135	1.42	109.00	7.68	3.345	1.72	129.50	7.53				
3.140	1.38	106.50	7.72	3.350	1.61	130.00	8.07				
3.145	1.38	108.50	7.86	3.355	1.64	130.50	7.96				
3,150	1.47	104.60	7.12	3.360	1.63	133.40	8.18				

Figure A.21 Cone penetration test data from sounding C8 (8 of 13).

	The University of Adelaide Cone Penetration Test									
	Client: Dep	artment of Civ	vil and Enviro	nmental En	gineering					
Job	Details: PhD	Research								
Test	ocation: C8									
Surfa	ce R.L.: 40.9	11 m AHD	Date	: 24th July	, 1992	Time:	1:33 pm			
	Cone Tip Sieeve Friction Cone Tip						Friction			
Depth	Resistance	Friction	Batlo	Depth	Resistance	Friction	Batio			
(m)	g (MPa)	f (kPa)	E (%)	(m)	g (MPa)	f (kPa)	E (%)			
		• (KI U)	·R(70)		Se (C)	1. (vi u)	1 R (70)			
3.365	1.74	129.50	7.44	3.575	1.55	122.70	7.92			
3.370	1.69	133.40	7.89	3.580	1.54	118.80	7.71			
3.375	1.64	132.90	8.10	3.585	1.55	120.70	7.79			
3.380	1.64	138.30	8.43	3.590	1.54	120.20	7.81			
3.385	1.61	136.90	8.50	3.595	1.66	121.70	7.33			
3.390	1.51	136.90	9.07	3.600	1.63	121.20	7.44			
3.395	1.60	136.90	8.56	3.605	1.61	123.20	7.65			
3.400	1.63	142.20	8.72	3.610	1.64	116.80	7.12			
3.405	1.63	136.90	8.40	3.615	1.55	119.70	7.72			
3.410	1.63	138.80	8.52	3.620	1.60	119.70	7.48			
3.415	1.54	135.90	8.82	3.625	1.61	118.80	7.38			
3.420	1.5/	134.40	8.56	3.630	1.5/	115.80	7.38			
3.425	1.54	132.00	8.57	3.635	1.52	115.30	7.59			
3.430	1.54	131.00	8.51	3.640	1.63	114.90	7.05			
3.435	1.48	120.00	8.55	3.045	1.51	115.80	7.07			
3.440	1.60	119.70	7.48	3.650	1.48	115.30	7.79			
3.445	1.60	119.30	7.40	3.655	1.51	112.90	7.48			
3.450	1.50	120.70	0.05	3.000	1.40	112.40	7.49			
3.455	1.40	120.20	0.12	3.000	1.54	112.40	7.30			
3.400	1.45	09.70	6.54	3.675	1.50	116.90	7.63			
3.400	1.51	90.70 N/A	N/A	3 680	1.54	118.80	7.50			
3.475	1.34	N/A	N/A	3 685	1.01	124.60	7.07			
3 480	1.65	131.00	9.03	3 690	1.57	120.20	7.66			
3 485	1.40	141 70	9.77	3 695	1.60	118 80	7.43			
3 490	1.47	138.80	9.44	3,700	1.63	123.70	7.59			
3,495	1.48	139.80	9.45	3,705	1.69	119.70	7.08			
3.500	1.39	135.90	9.78	3,710	1.72	125.60	7.30			
3 505	1.39	132.90	9.56	3.715	1.80	121.70	6.76			
3.510	1.51	133.90	8.87	3,720	1.77	125.10	7.07			
3.515	1.42	133.40	9.39	3,725	1.86	131.50	7.07			
3.520	1.47	130.50	8.88	3.730	1.77	135.90	7.68			
3.525	1.38	129.00	9.35	3.735	1.77	134.90	7.62			
3.530	1.48	125.60	8.49	3,740	1.82	134.90	7.41			
3.535	1.48	127.10	8.59	3.745	1.86	142.20	7.65			
3.540	1.36	120.70	8.88	3.750	1.83	N/A	N/A			
3.545	N/A	122.70	N/A	3.755	1.86	142.20	7.65			
3.550	N/A	126.10	N/A	3.760	1.88	139.30	7.41			
3.555	1.14	123.70	10.85	3.765	1.86	136.90	7.36			
3.560	1.54	126.10	8.19	3.770	1.86	134.90	7.25			
3.565	1.57	126.10	8.03	3.775	1.77	145.20	8.20			
3.570	1.55	121.70	7.85	3.780	1.74	144.70	8.32			

Figure A.22 Cone penetration test data from sounding C8 (9 of 13).

	The University of Adelaide Cone Penetration Test											
	Client: Dep	artment of Civ	vil and Enviro	nmental En	gineering		<u>,</u>					
Job	Details: PhD	Research										
Test Lo	ocation: C8											
Surfa			Date	• 24th July	1992	Time: 1	1.33 nm					
Suna				n 2403 July	, 1992	1	1.00 pm					
Denth	Cone Tip	Sleeve	Friction	Denth	Cone Tip	Sleeve	Friction					
Deptn	Resistance	Friction	Ratio	Depth	Resistance	Friction	Ratio					
(m)	q _c (MPa)	ť, (kPa)	F _R (%)	(m)	q, (MPa)	f _e (kPa)	F _R (%)					
3.785	1.69	144.20	8.53	3.995	1.77	133.90	7.56					
3.790	1.69	149.10	8.82	4.000	1.69	138.80	8.21					
3.795	1.74	149.10	8.57	4.005	1.73	135.90	7.86					
3.800	1.69	152.00	8.99	4.010	1.74	134.90	7.75					
3.805	1.74	154.90	8.90	4.015	1.82	139.80	7.68					
3.810	1.77	161.30	9.11	4.020	1.80	140.80	7.82					
3.815	1.74	157.40	9.05	4.025	1.76	146.10	8.30					
3.820	1.80	154.90	8.61	4.030	1.77	140.30	7.93					
3.825	N/A	148.60	N/A	4.035	1.83	145.20	7.93					
3.830	1.//	150.00	8.4/	4.040	1.80	138.80	7.71					
3.835	1.69	152.50	9.02	4.045	1.86	145.20	7.81					
3.840	1.76	148.10	8.41	4.050	1.74	144.20	8.29					
3.040	1.72	143.70	0.35	4.055	1.83	148.10	8.09					
3.000	1.09	142.20	0.41	4.000	1.00	145.70	7.75					
3.860	1.70	134.90	7.98	4.005	1.88	145.20	7.02					
3 865	1.65	134.90	8 13	4.075	1.00	143.20	8.00					
3.870	1.79	132.90	7.42	4.080	1.88	139.80	7 44					
3.875	1.69	133.40	7.89	4.085	1.80	141.30	7.85					
3.880	1.70	129.00	7.59	4.090	1.80	137.30	7.63					
3.885	1.79	131.50	7.35	4.095	1.86	135.40	7.28					
3.890	1.85	129.00	6.97	4.100	1.85	135.90	7.35					
3.895	1.79	128.10	7.16	4.105	1.73	140.30	8.11					
3.900	1.77	130.00	7.34	4.110	1.82	145.20	7.98					
3.905	1.70	123.70	7.28	4.115	1.80	143.20	7.96					
3.910	1.69	125.10	7.40	4.120	1.85	145.20	7.85					
3.915	1.73	125.60	7.26	4.125	1.88	138.30	7.36					
3.920	1.66	123.70	7.45	4.130	1.83	144.20	7.88					
3.925	1.69	121.70	7.20	4.135	1.77	145.20	8.20					
3.930	1.63	124.10	7.61	4.140	1.77	141.30	7.98					
3.935	1.60	122.20	7.64	4.145	1.83	141.30	7.72					
3.940	1.61	121.20	7.53	4.150	1.86	142.20	7.65					
3.945	1.66	122.20	7.36	4.155	1.82	144.20	7.92					
3.950	1.01	121./0	7.96 7.50	4.160	1./2	148.10	8.61					
3.900	1.0/	120.00	7.98 7.90	4.100	1./4	146.10	8.40					
3.500	1.64	127.10	7.00	4.170	1.70	144.20	0.19					
3 970	1 74	125 60	7.30	4 180	1 70	144.70	0.04 R AR					
3 975	1 61	128 10	7.96	4.185	1.75	145 20	8.20					
3,980	1.63	132 90	8.15	4,190	1.80	142 20	7.90					
3.985	1.77	130.00	7.34	4.195	1.83	145.20	7.93					
3.990	1.69	133.90	7.92	4.200	1.77	145.20	8.20					

Figure A.23 Cone penetration test data from sounding C8 (10 of 13).

	The University of Adelaide Cone Penetration Test											
	Client: Depa	artment of Civ	il and Environ	mental En	gineering							
Job	Details: PhD	Research										
Tortic												
Pest Lu			Data	• 24+b July	1002	Time- 1	·33 om					
Suna	Ce R.L.: 40.9			. 24th July,	, 1992 T	1	.55 pm T					
Death	Cone Tip	Sleeve	Friction	Dopth	Cone Tip	Sleeve	Friction					
Depth	Resistance	Friction	Ratio	(m)	Resistance	Friction	Ratio					
(m)	q _c (MPa)	t, (kPa)	F _R (%)	(m)	q _c (MPa)	f, (kPa)	F _R (%)					
4 205	1.88	142.20	7.56	4.415	2.24	145.70	6.50					
4.210	1.86	148.10	7.96	4.420	2.20	150.00	6.82					
4.215	1.88	143.70	7.64	4.425	2.20	149.60	6.80					
4.220	1.89	141.70	7.50	4.430	2.11	148.10	7.02					
4.225	1.94	136.40	7.03	4.435	2.05	154.00	7.51					
4.230	1.91	137.80	7.21	4.440	2.07	152.00	7.34					
4.235	1.83	134.90	7.37	4.445	2.02	157.90	7.82					
4.240	1.91	140.30	7.35	4.450	2.08	157.40	7.57					
4.245	1.88	141.70	7.54	4.455	2.05	155.90	7.60					
4.250	1.79	144.20	8.06	4.460	2.02	154.90	7.67					
4.255	1.80	143.20	7.96	4.465	2.01	153.50	7.64					
4.260	1.77	146.10	8.25	4.470	1.94	149.10	7.69					
4.265	1.80	148.60	8.26	4.475	1.98	147.00	7.45					
4.270	1.83	148.10	8.09	4.400	1.90	144.20	7.30					
4.275	1.77	152.00	8.35	4.400	1.88	147.60	7.25					
4.200	1.02	157.40	8 79	4 495	1.00	143.70	7.52					
4 290	1.75	170 10	9.15	4.500	1.88	143.70	7.64					
4 295	1.88	160.30	8.53	4.505	1.92	143.70	7.48					
4.300	1.94	N/A	N/A	4.510	1.94	143.20	7.38					
4.305	1.82	157.40	8.65	4.515	1.83	148.60	8.12					
4.310	1.77	150.00	8.47	4.520	1.91	148.60	7.78					
4.315	1.80	144.20	8.01	4.525	1.98	146.60	7.40					
4.320	1.80	136.90	7.61	4.530	2.02	143.70	7.11					
4.325	1.74	142.20	8.17	4.535	1.94	143.20	7.38					
4.330	1.85	139.80	7.56	4.540	1.96	141.70	7.23					
4.335	1.77	139.80	7.90	4.545	1.92	140.80	7.33					
4.340	1.73	140.30	8.11	4.550	1. 99	141.30	7.10					
4.345	1.64	134.90	8.23	4.555	1.88	145.20	7.72					
4.350	1.79	134.90	7.54	4.560	1.92	144.20	7.51					
4.355	1.83	142.70	7.80	4.565	1.96	144.20	7.36					
4.360	1.86	143.20	7.70	4.570	1.94	150.00	7.73					
4.365	2.05	146.60	7.15	4.575	1.95	150.00	7.69					
4.370	2.13	144.70	6.79	4.580	1.96	155.90	7.95					
4.375	N/A	143.20	N/A	4.585	1.94	157.90	0.14					
4.380	2.23	145.20	0.51	4.590	1.90	150.90	7.04					
4.385	2.1/	144.20	0.00	CCC.P	1.34	104.00	7.54 8.48					
4.390	2 12	149.10	6.05	4 605	1 95	158.40	8 12					
4.393	2.13	140.10	0.55 8 80	4 610	1.00	155.90	7.87					
4.400	2.17	148 10	7.22	4.615	1,99	158.40	7.96					
4.410	2.11	147.60	7.00	4.620	2.08	156.40	7.52					

Figure A.24 Cone penetration test data from sounding C8 (11 of 13).

	The University of Adelaide											
				one pen	eurauon	Iest						
		Client: Dep	artment of Ci	vil and Enviro	nmental Er	ngineering						
	Job	Details: PhD	Research									
	Test L	ocation: C8										
	Surfa	ice B.L.: 40.9		Date	• 24th July	1992	Time	1.33 pm				
		T	Т		ग ग	, 1552 T		T.55 pm				
	Depth	Cone Tip	Sleeve	Friction	Depth	Cone Tip	Sleeve	Friction				
	(m)	Resistance	Friction	Ratio	(m)	Resistance	Friction	Ratio				
	()	q _c (MPa)	f, (kPa)	F _R (%)	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	q _c (MPa)	f _s (kPa)	F _R (%)				
	4.625	2.01	156.40	7.78	4.835	2.32	155.90	6.72				
	4.630	1.99	153.50	7.71	4.840	2.36	156.40	6.63				
	4.635	1.99	155.40	7.81	4.845	2.33	157.90	6.78				
	4.640	1.94	154.00	7.94	4.850	2.29	159.80	6.98				
	4.645	1.95	156.40	8.02	4.855	2.35	156.90	6.68				
	4.650	2.01	151.00	7.51	4.860	2.39	157.40	6.59				
	4.655	1.96	150.50	7.68	4.865	2.36	158.40	6.71				
	4.660	1.94	152.00	7.84	4.870	2.33	156.40	6.71				
	4.665	1.96	156.90	8.01	4.875	2.38	155.40	6.53				
	4.670	1.99	164.20	8.25	4.880	2.32	151.50	6.53				
	4.675	1.91	169.10	8.85	4.885	2.36	142.20	6.03				
	4.680	1.96	172.50	8.80	4.890	2.35	141.30	6.01				
	4.685	1.98	171.10	8.64	4.895	2.35	165.20	7.03				
	4.690	1.99	171.10	8.60	4.900	2.29	169.60	7.41				
1	4.695	1.94	N/A	N/A	4.905	2.24	171.60	7.66				
	4.700	1.99	169.10	8.50	4.910	2.23	173.00	7.76				
	4.705	2.04	167.20	8.20	4.915	2.20	172.00	7.82				
1	4./10	2.04	169.10	8.29	4.920	2.14	171.60	8.02				
I	4./15	2.04	171.10	8.39	4.925	2.18	171.10	7.85				
	4.720	2.05	164.20	8.01	4.930	2.20	170.60	7.75				
1	4.725	1.94	164.20	8.46	4.935	2.20	170.60	7.75				
I	4.730	1.95	163.20	8.37	4.940	2.27	170.10	7.49				
I	4.735	1.99	164.20	8.25	4.945	2.20	172.50	7.84				
	4./4U 1 715	2.04	163.20	8.00	4.950	2.23	175.00	7.85				
	4.740	4.14 2.20	160.80	7.51	4.955	2.23	1/1.10	7.67				
	4.755	2.20	157.40	7.01	4.900	2.08	1/2.50	8.29				
	4.750	2.20	157.90	1.10	4.905	1.92	1/0.10	8.86				
	4 765	2.32	154.90	0.00	4.9/U	2.04	164.20	8.05				
l	4 770	2.52 N/A	150.40	0.74 N/A	4.9/5	2.17	153.50	1.07				
l	4 775	2 20	154.00	7.00	4.500	2.20	143.2U	0.51				
l	4,780	2.20	155 90	7.00	4 900	2.14	N/A	PV/A N//A				
L	4,785	2.24	154 00	88.3	4 005	2.20	NVA NI/A	IWA N/A				
ŀ	4,790	2.23	154.00	6.00	5 000	2.14 2.14	N/A	IVA N/A				
	4.795	2.23	153.00	6.86	5.005	208	N/A	N/A				
	4.800	2.26	154.00	6.81	5.010	2.11	N/A	N/A				
	4.805	2.26	152.00	6.73	5.015	2.14	N/A	N/A				
	4.810	2.29	153.00	6.68	5.020	2.14	N/A	NA				
	4.815	2.23	154.40	6.92	5.025	2.11	N/A	N/A				
ĺ	4.820	2.39	154.00	6.44	5.030	2.16	N/A	N/A				
	4.825	2.38	150.00	6.30	5.035	2.14	N/A	N/A				
	4.830	2.40	158.40	6.60	5.040	2.08	N/A	N/A				

Figure A.25 Cone penetration test data from sounding C8 (12 of 13).

	The University of Adelaide Cone Penetration Test											
doL	Client: Depa Details: PhD	artment of Civ Research	il and Environ	mental En	gineering		<u>, , , , , , , , , , , , , , , , , , , </u>					
Test Lo	cation: C8		Data	- 24th July	1002	Time 1	·33 nm					
Depth (m)	Cone Tip Resistance q. (MPa)	Sieeve Friction f, (kPa)	Friction Ratio F _R (%)	Depth (m)	Cone Tip Resistance q. (MPa)	Sleeve Friction f, (kPa)	Friction Ratio F _R (%)					
5.045 5.050 5.055	Q _c (MP2)	N/A N/A N/A	Γ _R (<i>π</i>) N/A N/A N/A									

Figure A.26 Cone penetration test data from sounding C8 (13 of 13).



Figure A.27 Cone penetration test results from sounding C10.



Figure A.28 Cone penetration test results from sounding CD1.



Figure A.29 Cone penetration test results from sounding CD30.



Figure A.30 Cone penetration test results from sounding CD40.



Figure A.31 Cone penetration test results from sounding D5.



Figure A.32 Cone penetration test results from sounding D8.



Figure A.33 Cone penetration test results from sounding E1.



Figure A.34 Cone penetration test results from sounding E7.



Figure A.35 Cone penetration test results from sounding G0.



Figure A.36 Cone penetration test results from sounding G5.



Figure A.37 Cone penetration test results from sounding G10.



Figure A.38 Cone penetration test results from sounding H7.



Figure A.39 Cone penetration test results from sounding H10.



Figure A.40 Cone penetration test results from sounding I1.



Figure A.41 Cone penetration test results from sounding I9.



Figure A.42 Cone penetration test results from sounding J8.



Figure A.43 Cone penetration test results from sounding K0.



Figure A.44 Cone penetration test results from sounding K10.

APPENDIX B

ENGINEERING BOREHOLE LOGS

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B.1 INTRODUCTION

The following engineering borehole logs detail the soils encountered in the nine boreholes drilled at the South Parklands site. In describing the moisture condition and consistency of the soils encountered, a standard notation has been used, which is detailed below.

• Moisture condition of the soil is based on its appearance:

D	Dry	Looks and feels dry; cohesive soils are usually hard, powdery or friable, granular soils run freely through hands.
Μ	Moist	Soil feels cool, darkened in colour; cohesive soils usually weakened by moisture, granular soils tend to cohere, but one gets no free water on hands on remoulding.
W	Wet	Soil feels cool, darkened in colour; cohesive soils weakened, granular soils tend to cohere, free water collects on hands when remoulding.

• **Consistency** is based on the unconfined compressive strength (UCS) of the soil which is usually estimated, or measured by a hand penetrometer:

Symbol:	VS	S	F	St	VSt	Н
Term:	Very Soft	Soft	Firm	Stiff	Very Stiff	Hard
UCS (kPa):	0 - 25	25 - 50	50 - 100	100 - 200	200 - 400	> 400

If the soil crumbles during the test, without a meaningful result, it is described as **friable** (**Fb**).

BOREHOLE A0

Drilling Method: Dynamic-push

Date Drilled: 15th August 1992

Depth (m)	USCS	Description	Moisture	Consistency
		Sandy CLAY/Clayey SAND, low		
0.0 - 0.4	CL/SC	plasticity, dark brown. Fine to	М	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
0.4 - 1.7	CL/CH	plasticity, pale brown. Fine to	М	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
1.7 - 2.3	CH	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
2.3 - 5.0	CH	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE A10

Drilling Method: Solid-Flight Auger

Date Drilled: 26th February 1993

Depth (m)	USCS	Description	Moisture	Consistency
		Sandy CLAY/Clayey SAND, low		
0.0 - 1.1	CL/SC	plasticity, dark brown. Fine to	М	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
1.1 - 1.6	CL/CH	plasticity, pale brown. Fine to	М	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
1.6 - 3.4	CH	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
3.4 - 5.0	CH	green with red-brown and yellow	Μ	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE C2

Drilling Method: Dynamic-push

Date Drilled: 15th August 1992

Depth (m)	USCS	Description	Moisture	Consistency
		Sandy CLAY/Clayey SAND, low		
0.0 - 0.7	CL/SC	plasticity, dark brown. Fine to	М	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
0.7 - 1.1	CL/CH	plasticity, pale brown. Fine to	М	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
1.1 - 2.3	СН	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
2.3 - 5.0	CH	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE C8

Drilling Method: Dynamic-push

Date Drilled: 15th August 1992

Depth (m)	USCS	Description	Moisture	Consistency
0.0.02		Sandy CLAY/Clayey SAND, low	М	T 1-
0.0 - 0.2	CL/SC	plasticity, dark brown. Fine to	IVI	FD
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
0.2 - 0.9	CL/CH	plasticity, pale brown. Fine to	Μ	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
0.9 - 1.1	CH	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
1.1 - 5.0	СН	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE F5

Drilling Method: Dynamic-push

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Date Drilled: 15th August 1992
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Depth (m)	USCS	Description	Moisture	Consistency
		Sandy CLAY/Clayey SAND, low		
0.0 - 0.3	CL/SC	plasticity, dark brown. Fine to	М	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
0.3 - 0.9	CL/CH	plasticity, pale brown. Fine to	М	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
0.9 - 1.6	CH	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
1.6 - 5.0	CH	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE I2

Drilling Method: Dynamic-push

Date Drilled: 15th August 1992

Depth (m)	USCS	Description	Moisture	Consistency
		Sandy CLAY/Clayey SAND, low		
0.0 - 0.5	CL/SC	plasticity, dark brown. Fine to	М	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
0.5 - 1.8	CL/CH	plasticity, pale brown. Fine to	М	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
1.8 - 2.4	CH	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
2.4 - 5.0	CH	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE I8

Drilling Method: Dynamic-push

Date Drilled: 15th August 1992

Depth (m)	USCS	Description	Moisture	Consistency
		Sandy CLAY/Clayey SAND, low		
0.0 - 0.2	CL/SC	plasticity, dark brown. Fine to	Μ	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, high plasticity,		
0.2 - 1.0	CL/CH	brown with black and pale brown.	М	Fb
		Fine to medium sand.		
		Transitional Member		
		Silty Sandy CLAY, high plasticity,		
1.0 - 2.2	CH	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
2.2 - 5.0	CH	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE K0

Drilling Method: Dynamic-push

Date Drilled: 15th August 1992

Depth (m)	USCS	Description	Moisture	Consistency
		Sandy CLAY/Clayey SAND, low		
0.0 - 0.5	CL/SC	plasticity, dark brown. Fine to	М	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
0.5 - 2.0	CL/CH	plasticity, pale brown. Fine to	М	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
2.2 - 3.3	СН	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
3.3 - 5.0	CH	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		

BOREHOLE K10

Drilling Method: Dynamic-push

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Date Drilled: 15th August 1992
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Depth (m)	USCS	Description	Moisture	Consistency
0 0 0 0		Sandy CLAY/Clayey SAND, low		I
0.0 - 0.3	CL/SC	plasticity, dark brown. Fine to	Μ	Fb
		medium sand. Trace of root fibre.		
		Callabonna Clay		
		Silty Sandy CLAY, medium		
0.3 - 1.6	CL/CH	plasticity, pale brown. Fine to	М	Fb
		medium sand. Extremely calcareous.		
		Calcareous Mantle		
		Silty Sandy CLAY, high plasticity,		
1.6 - 2.0	CH	white to grey. Fine to medium sand.	М	Fb
		Calcareous.		
		Limy surficial layer.		
		Silty CLAY, high plasticity, grey-		
2.0 - 5.0	CH	green with red-brown and yellow	М	VSt/H
		mottling. Some fine sand.		
		Keswick Clay		
APPENDIX C

DATA BASE OF THE GEOTECHNICAL **PROPERTIES OF THE KESWICK AND HINDMARSH CLAYS**

C.1 INTRODUCTION

The following pages provide a brief overview of the *KESWICK* data base, which contains geotechnical properties of the Keswick and Hindmarsh Clays. Only part of the data base is shown, as an example of the information contained within it. Two columns, which contain information regarding internal job and borehole numbers relevant to each site investigation, have been hidden in order to provide some anonymity for the consulting practices and government instrumentalities who provided data for this research.

The following pages are organised in the order in which the data were obtained by the author, that is:

- 1. Coffey Partners International Pty. Ltd.;
- 2. Rust PPK Consultants Pty. Ltd. (formerly PPK Consultants Pty. Ltd.);
- 3. SACON (South Australian Department of Housing and Construction);
- 4. Golder Associates Pty. Ltd. (formerly Woodburn Fitzhardinge Geotechnical);
- 5. ACER Wargon Chapman (SA) Pty. Ltd. (formerly Hosking Oborn Freeman and Fox);
- 6. Koukourou and Partners;
- 7. Connell Wagner (SA) Pty. Ltd.;
- 8. Kinhill Engineers.

C.2 NOTES ON DATA

- The *Soil Layer Tested* column refers to the soil type (K: Keswick Clay; S: Hindmarsh Clay Sand Member; L: Hindmarsh Clay Layer; and K/L: Undifferentiated Keswick Clay/ Hindmarsh Clay Layer) to which the particular test refers.
- The data, whose title is given in *italics*, are *derived* from measured data by means of commonly applied phase relationship equations. These include:

$$\gamma_d = 9.81 \times \rho_d \tag{C.1}$$

$$\gamma = \gamma_d (1+w) \tag{C.2}$$

$$e = \frac{G_s \gamma_w}{\gamma_d} - 1 \tag{C.3}$$

$$S_r = \frac{w\gamma_d G_s}{G_s \gamma_w - \gamma_d} \tag{C.4}$$

$$G_s = \frac{\gamma_d}{\gamma_w - w\gamma_d} \quad \text{(for } S_r = 100\%\text{)} \tag{C.5}$$

Table C.1Data from Coffey Partners International Pty. Ltd.

Rei No	AMG North.	Coords. East.	Surface RL (m) (AHD)	Earth b	• Teo of j Sead	Lower	Depth to Dottom of Layer (m)	Test Type	Test Dept (m)	Sell Layer Toria	Undrainer Shear Strength ss (kPa)	Confining Pressure (kPa)	Undrained Young's Modulus (NGPa)	Undrained Shenr Strungth es (hPa)	Internal Angle of Priction (degree)	Dry Dunsity (Va3)	Dry Unit Weight (hNim3)	Water Contest (%)	Total Suction (pF)	Bulk Unit Weight (kN/m3)	Vold Ratio	Degree 4 Saturation (%)	Back- Calculated Specific Gravity	Coeff. of Earth Pressure at Rest	lastab Biy laster (%)	SPT Depth (m)	Data N	Saman' Yaar	Lecation	Comments	Assumed Constants and Legend
2 2 1	32473 32473 32490	90560 90560 90550 90559	45.25 45.25 45.06	2.7 2.7 2.9	Caller Pr 9.0 9.1	13.0 13.0 13.2 13.2	17.1 17.1 17.3	SPLT SPLT SPLT	No. 1 5.43 4.10 5.47	K			65 105 100	129 125 129				33.3 28.2 33.8	4.00									A/1996 A/1996 A/1996	State Benk Building (Bensheiss located mer the end of Sevings Bank Place, severes Son was of King	Laver decide interpolated between BH1 and BH2 Adi to BH1 Adi to BH1	Specific Cravity, C = 2.7
1 3 3 3 3 3	32463 32463 32463 32463	80561 80561 80561 80561	45.45 45.45 45.45 45.45	2.5 2.5 2.5 2.5 2.5	1.9 1.9 1.9	14.6 14.6 14.6	16.9 16.9 16.9	SPET SPET SPET SPET	4.50		100	150	375 90	100		144	14.13	32.7		18.75	0.98	100.90	2.72	4.4		11.9	17	A/1986	William St.)	Ba suspect	Test Types: SFLT = Screw Plate Lead Test. SBFT = Solf Boring
7	32463 32490 32490 32490 32490	80559 80559 80559 80559	45.45 45.06 45.06 45.06	2.5 2.9 2.9 2.9	8.9 9.1 9.1 9.1	14.6 12.2 12.2 12.2	16.9 17.3 17.3 17.3	SIMPT TUU1 TUU1 TUU3	16.10 3.15 4.65 5.70	D L K K	200 120 130	120 180 200	220	300 200 120 125	0	1.55 1.42 1.47	15.21 13.93 14.42	26.9 33,4 30.8		19.30 18.58 18.86	0.74 0.90 0.84	97.99 100.04 99.39	2.70	3.5		10.0	37	A/1986		Transitional Member	Pressummeter Test. CPT = Cone Penetration Test. TUU# = Triaxial,
	32480 32480	80559 80559	45.06 45.06	2.9	9.1 9.1	12.2 12.2	17.3	דטטז דטטו	7.15	K 5 L	127 121 200 280	344 470 280 300		200		1.52	14.91 14.52	30.6 31.5		<u>19.47</u> 19.09	0.78 0.82	106.43 103.18	2.84			_11.5					Unconsolidated, Undrained unt with # stages. TCD# = Triaxial, Consolidated, Drained
	32490	80523	45.06 39.93	0.0	4.8	9.0	17.3		13.2	р <u>Г</u> К	272 269 262 155	309 633 926 70	18	125	7.5	1.59	15.60	28.2 28.1		19.68	0.70	<u>101.33</u> 97.73	2.73			5.0	36	Sp/1986	State Bank Building		TUC = Triaziel, Unconfined Compression Test. DST = Direct Shear Test.
	32458	80523	39.93	0.0	4.8	. 9.0	12.3		3.62	ĸ	167 165 187 212 237	140 280 140 280	м	140	8.5	1.65	16.19	22.7		19.86	0.64	96.31				7.5 9.9 10.2	2 22 22 23 23 23 23 23 23 23 23 23 23 23				Sensons: S = Summer
5	32488	80520	39.85	0.0	3.8	8.0	12.0	TUU3	1.92	ĸ	71 80 106 212	75 150 300	53 	50	7.5	1.60	15.70	24.8		19.59	0.69	97.40 69.46				3.9 5.0 6.5	35 45 >50	3 p/1986		Transitional Member	A = Aubumn Sp = Spring W = Winter
5	32488 32851	80520 81223	<u>39.85</u> 44.10	0.0	3.8	8.0	12.0	τυυι	8.70	L	313 465 232	280 560 300	73	232		1,46	14.32	31.7		18.86	0.85	100.78	2.72						Cay Munal Building	Prom a Dames & Moore report	
7 8 9 10	32849 32848 32875 32875 32873	\$1194 \$1169 \$1220 \$1200	44.10 44.10 43.90 44.00	4.9 5.2 4.9 4.9			8.5 10.1 7.6 11.3	;																					Car. Pulismoy St. & North Tes.		
11 12 13 14	32870 32658 32770 32497	81169 80555 80876 80797	44.00 43.50 44.80 45.10	4.9 2.0 2.0 4.0			11.3 14.3 17.4 15.2																						9 Hindley St. 90 Rundle Mail SW cur Gawler PI & Graefell St. Lindley St.		
16 17 18	31764 31220 32475 32306	80719 79675 80920 81225	45.30 40.10 46.00 47.30	3.2 1.3 3.1 2.0	9.0	12.5																							Car Carriageon & K. William Sts Car. West & South Tess. 101-107 Grounfell St. Car. Pubeney & Flinders Sts.	SL Pauls Redevelopment	
20 21 21 21	32391 32489 32489 32489	80168 80354 80354 80354	43.60 43.04 43.04 43.04	2.0 1.5 1.5	6.9 6.9 6.2	9.6 9.6 9.6	15.4 15.4 15.4	SPLT TUUI TUUI	2.50 1.63 3.15	K K	125 120	65 128	36	75 125 120		<u>1.51</u> 1.37	<u>14.81</u> 13.44	29.0 36.0	3.10 3.40	<u>19.11</u> 18.28	0.79	99.36 100.12	2.70		2.7	8.5	29	A/1984	Car. Light Sq. & Playhouse Lane Common weakth Contre Car. Currie & Topham Str.		
21 22 23 23	32489 32498 32465 32465	80354 80423 80388 80388	43.04 43.08 43.99 43.99	1.5 1.0 1.6 1.6	6.9 5.8	9.6 10.5	15.4 15.5 14.0 14.0	TUUI SPLT SBPT	5.15 2.50 2.75	к К/L К/L	170	210	<u>84</u> 10	170 128 75		1.47	14.42	30.7	4.20	18.85	0.54	99.06		5.7				A/1984		Suspect En & Ko	
23 23 23 23	32465 32465 32465 32465	80388 80388 80388 80388 80388	43.99 43.99 43.99 43.99	1.6 1.6 1.6 1.6			14.0 14.0 14.0 14.0	SBPT SPLT SBPT SBPT	5.00 5.40 7.50 10.50	КЛ. КЛ. КЛ.			55 196 65 84	100 136 175						·				4.2 4.1 5.5						Suspect Eu	
24 25 26 27	32434 32444 32803 32779	80360 80418 81491 81528 80361	44.52 44.62 41.90 42.00	3.2 2.6 7.0 7.0			16.1 14.8 >7.8 >7.5	TUUI	6.15	KA.	160	255		160		1.47	14,42	31.4	4.20	18.95	0.84	101.32	2.73		3.7			A/1984	East End Market		
29 30 31	32414 32430 32415 32415	80355 80403 80405 80405	44.10 44.10 44.10 44.10	4.0 4.0 3.5 2.4 2.4					5.21 5.20 3.20	KAL KAL KAL	93 110 83 95 64	100 100 60	32 32 40 24 28	95 95 44		1.41 1.49 1.44 1.40	13.83 14.62 14.13 13.73 13.91	31.0 33.1 34.7 34.0	3.40	18.60 19.15 18.80 18.50	0.91	101.82 103.07 102.14 100.90	2.77 2.75 2.72 2.75					A/1984 A/1984 A/1984 A/1984	Che. Waymouth and Topham Sis.		
32 33 33 34	32434 32416 32416 32463	80465 80465 80465 80465	44.10 44.10 44.10 43.90	3.8 2.4 2.4 2.6	9.0	>12		TUU1 TUU1 TUU1 TUU1	5.20 3.15 5.20 3.20	KA. KA. KA.	75 140 86 75	100 60 100 60	14 25 28 36	75 140 86 75		1.37 1.41 1.41 1.41	13.44 13.83 13.83 13.83	36.1 31.1 33.7 33.8		18.29 18.13 18.49 18.51	0.97 0.91 0.91 0.91	100.40 91.78 99.45 99.75	2.71	-		-		A/1984 A/1984 A/1984			
34 35 36 37	32463 30710 30661 30688	80465 81578 81581 81553	43.90 45.90 45.90 45.80	2.6 4.5 3.8 5.5	9.0	>12	>6.2 >6.4 >6.4	TUUI	5.20	ĸ	107	100	60	107		1.46	14.32	32.1		18.92	0.85	102.05	2.75						Car, Greenhill Rd. & Porter St.		
38 39 40	31790 32548 33128	80201 81268 81054	42.50 46.30 29.90	2.0 3.6 1.5			>6.0 2.8	דטטו דטטז	4.95	KA.	165 225 220	100 50 100		165 225	0	1.46 1.50	14.32 14.72	31.6 29.3	4.02	18.85 19.03	0.85	100.46	2.71					A/1984 A/1984	Chr. 1 nothes SL & Wright Cl. Chicorn, Hindmarth Sg. Uni. of Adelaide Barr Smith Library Pootbridge	Upper level	
41 42 43	32649 31990 31969	81294 80305 80306	44.80 43.30 43.20	3.0 3.3 26			>5.6 >5.8 >4.6	דטטו	4.35	KA	70	80		70		1.47	14.42	31.4		18.95	0.84	101.32	2.73					\$/1984.5	Beni Street Carpark Moonia Street Carpark Moonia St.		
45	31951	80365 80358	43.50	1.8 2.7			>5.0	τυυι	3.25	КЛ.	90	60		90		1.33	13.05	37.4		17.93	1.03	98.03						S/1984,5			

Table C.2Data from Rust PPK Consultants Pty. Ltd.

											. 16							-				Demo	Bash	Co	Indah	1 59-7	Deta				
	AMG	Ceerds.	Surface	Depth to	Tep of 1	ayer (m)	Depth to			Sell	Undrained	Confining	Undrained	Undrained	Internal	Dry	Dry	Water	Total	Bulk Link	Vall	, Degree	Sect-	of Rarth	Laping-	Denth		Sensor/	Location	Comments	Assumed Constants
Rd.			RL			1. 1	Bottom	Test	Test	Layer	Shear	Pressure	Young's	Sheer Finneth	Angle of Printing	(MmS)	Wataba	(%)	(aD)	Weinle	Batta	Saturation	Smalle	Presere	Index	(m)	N	Year			and Legend
Ne.	North.	Best.	(m)	Kerwick	Saud	Lower	af Layer	Type	Depth	Tested	Strength	(1046)			(desreet)	(0	(kNim3)	(/		(kN/m3)		(%)	Gravity	at Rest	(%)						
┝╍╍┵			(AHD)	1						<u> </u>	BU (MPW																				
L	D	ala Sourc		1.4	PT1		16 e		T																	10.1	48	W/1988	Commonwoalth Law Courts		Specific
166	31766	80630	44.60	1.2	9.5	10.5	12.4																			· · · ·			Car. King William & Wright Sts.		Gravity,
167	31768	80636	44.70	2.0	10.0	1.10.3			1.50	KA.															4.3			W/1988		Core Shrinkage Method	G=
	31/22	80636	44.70	<u></u>			~~		4 10	KA.															4.2						
100	31/33		44.70						7.70	KA.															4.2						Test Types:
	31733	40634	44.70	20		10.6	>13.25	TCUB	7.15	X	114	75	15	110	2	1.29	12.65	36.3	3.78	17.25	1.09	89.67						W/1968			SPLI = SCOW FIRM
	31/01				7.8		2 1 2 1 2 2		1		116	150											·								SDRT - Solf Baring
\vdash							-		1		117	300																			Bu company Test
160	31781	80638	44.70	20	9.2	10.6	>13.25	TCU3	10.75	L	219	100	10	195	3.5	1.65	16.19	19.5	3.36	19.34	0.64	\$2.74									CTT - Core Prostration
H##	21/21		1 10.00								219	200													<u> </u>						Test
			1	1					1		244	400													<u> </u>						TIJIM - Triazia).
160	31781	80638	44.70	2.0	9.2	10.6	>13.25	TCU3	13.15	L	181	150	21	165	2	1.36	13.34	34.5	3.29	17.94	0.99	94.54			<u> </u>	1					Unconsolidated Undrained
⊦ ‴†			1 100						T		190	300									$ \rightarrow $			<u> </u>		ł					that with it stant.
			1	1					L		200	600						ļ	<u> </u>	<u> </u>	┝─┥			├	I	 	<u> </u>				T(Di a Triazia)
170	31767	80646	44.70	2.0	9.2	10.6	>13.25	SPLT	3.25	K			71	120					<u> </u>		\vdash			├				W/1986			Consolidated Drained
170	31767	80646	44.70	2.0	9.2	10.6	>13.25	SPLT	5.38	K			62	112							┝──┤			<u> </u>		 		Without			mat with # stans.
171	31772	80634	44.70	2.0	9.2	10.6	>13.25	SPLT	4.28	K			100	121							┣━━┦					+	<u> </u>	W/1966			TUC = Trianial.
171	31772	80634	44.70	2.0	9.2	10.6	>13.25	SPLT	7.38	K			82	176					<u> </u>		┝─┤					<u>+</u>			Muse BEMM Providence		Unconfined Compression
172	32754	79994	44.20	5.5			10.8		\vdash										í		┝╼╼┥					1	├ ──┤		ASSE Development		Test.
173	32852	80336	29.00	N/B																	┝─┤			<u> </u>	I				VICK PARKING		DST = Direct Shear TeaL
174	32845	80239	29.00	5.5			16.7		1											<u> </u>	┝──┤				 	1	<u> </u>				
175	32827	80112	30.10	4.3	9.8	10.7	16.7		I									·			\vdash		— —	<u> </u>	<u> </u>	1 1					
176	32887	80085	28.70	N/E														-			┝┈╼╋										Sensons:
177	32958	80105	27.70	N/B							<u> </u>										$ \rightarrow $			i	 						S - Summer
178	32847	80270	28.80	N/E								ļ																			A = Aupumn
179	32913	80268	28.60	N/B														ļ			-+	_		-		1					Sp = Spring
180	32975	80271	28.10	N/E																10.01		102 64	3.76					Sn/1073	Education Dant, Building	Triaxial tasts performed on	W - Winter
181	32174	80944	45.80	2.6	11.7	13.1	18.4	TUU	7.35	K	156	138	69	138	4	1.421	13.94	34.2		18./1	0.90	102.30	374		<u> </u>			SM 1 1 1 3	Cor. Flinders St. & Gawler Pl.	actuarate suttities	
181	32174	80944	45.80	2.6	11.7	13.1	18.4	τυυ	7.35	ĸ	200	276	62			1.423	13.96	. 34.9		10./1	0.90	104.39	2.0		<u> </u>		1			(TechSearch testing from	
181	32174	80944	45.80	2.6	11.7	13.1	18.4	Τυυ	7.35	K	154	69	35			1.432	14.05	34.2		18.65	0.87	87.11	<u></u>			1				DME bores)	
181	32174	80944	45.80	2.6	11.7	13.1	18.4	Τυυ	7.35	K	185	414	54			1.461	14.33	30.5		18.70	0.83	97.11				1					
181	32174	80944	45.80	26	11.7	13.1	18.4	τυυ	7.35	K	160	104					14.46	20.0	<u> </u>	10,00	0.84	99.76			1						
181	32174	80944	45.80	2.6	11.7	13.1	-18.4	TUU	7.35	ĸ	196	207	- 54			1,400	14.39	31.1		18.03	0.87	88 33			<u> </u>			Sp/1973			
182	32230	80932	45.70	4.0	10.6	12.1	18.7	TUU	9.30	K.	259	138	41	165	3.5	1.444	14.17	32.0		18.70	0.07	00 33					1	-			
182	32230	80932	45.70	4.0	10.6	121	18.7		9.30	X	234	276	- 54			1.464	19.17	32.0		10.79	0.01	101 12	2.73								
182	32230	80932	45.70	4.0	10.6	121	18.7		9.30	K.	245	552	42			1,430	19,49	300		18.85	0.83	en 12									
182	32230	80932	45.70	4.0	10.6	121	18.7	TUU	9.30	K	217	69	41			1.4/2	14.77	310		10.00	0.86	97 82		1							
182	32230	80932	45.70	4.0	10.6	12.1	18.7	TUU	9.30	K .	203	207	52	<u> </u>		1 476	14 51	30.0		18.96	0.83	98.12		1			1				
182	32230	80932	45.70	4.0	10.6	12.1	18.7		9.30	<u> </u>	262	690	/2	120		1 424	14 07	27.0		19.01	0.77	94.76									
182	32230	80932	45.70	4.0	10.6	121	18.7		14.15	<u> </u>	241	2/0	<u> </u>	+ · · · · · · · · · · · · · · · · · · ·	╞╴╩╴	1.526	14 07	27.0	<u> </u>	19.01	0.77	94.76		1							
182	32230	80932	45.70	4.0	10.6	1 12.1	18.7		14.15	<u> </u>	154	156	62	<u>├</u> '		1.526	14.97	27.0	<u> </u>	19.01	0.77	94,76		1	1						
182	32230	80932	45.70	4.0	10.6	12.1	18.7		14.15		270	222	81	<u> </u>		1,455	14.22	31.0		18.70	0.86	97.82		1							
182	32230	80932	45.70	4.0	10.6	121	18.7	100	+ 14.15	4 -	10			 		1.777	1	1								11.5	>50		122 Piris St.		
183	32390	\$1106	46.40	1.5	11.2	122	>124	 	+	╉╼╼┥		<u> </u>	·	<u> </u>		t	1	t		1									Playhouse Lans Carpark		
184	32454	80196	42.30	2.5	ł	╂───┤	7.5	 	+	+		┼───		t		1	1	t													
185	32430	80234	43.10	20		+	14.0	<u> </u>	+			+		h		 	1	t											102-106 North Tcs.		
186	32784	80187	31.90	N/E	 	+		+	+			+		t			1	1													
187	32757	80236	33.60	N/E	 			 		1	<u> </u>	+		1		i	1	1			rt								Kintore Ave.		
188	33253	80824	27.60	N/E	 	┢┈╴┨		<u> </u>	+	1		+		<u>├</u>		<u>├</u>	1	†		h				I					North Tco., Morphett, Hindley &		
189	32695	80163	35.40	4.5	ł		6.1	+	+	4	——	1	<u> </u>	t		t	1	1	t										Victoria Sta.		
190	32696	80104	35.00	N/B		┟──┥		+	+	1 1		+	l	t	<u> </u>	<u> </u>	<u> </u>	1	1												
191	32709	80066	34.10	27			6.3	<u> </u>	+	1		+	┢────	 	t	i —	<u>+</u>	t	<u> </u>	<u> </u>											
192	32695	80223	36.00	1 24	1	+	0.1	-	1			t	100	100	t	1	1	1	1	r			Г			11.5	>50	A/1989	17 Angas SL		
193	31829	80856	45.80	2.9	11.0	12.3	20.7	SPLT	4.20			1	100	140	<u> </u>		<u> </u>	1	T												
193	31829	80856	45.80	2.9	11.0	12.3	20.7	SPLT	17.20	4-		1	1.00	+		t	<u> </u>	1		1									Car. Pirie St. & Gewler PL		
194	32371	80653	46.00	1.8	10.4	10.6	>10.7	├ ──	+	1		+	<u> </u>	t	 	1	<u> </u>	t	t	1						1			Car. Plinders & Prome Sts.		
195	32323	81348	47.30	2.0			>7.4	╂────	+	1	<u> </u>	<u> </u>	<u> </u>	<u> </u>	t	1	<u> </u>	t	t	1	tt		1			1			195 Greafell St.		L
196	32562	81426	45.10	1.5	Į	4	>6.6	l	+			<u> </u>	 	<u> </u>	l	†	t	1	t	1			l	T	I				Hindmansh Sq. (Aurora Hotel)		
197	32466	\$1282	46.40	22	<u> </u>	+			+	1 10		1	101	242	1	t —	1	1	t	1			<u> </u>					Sp/1983	89 Pinis SL		
198	32861	80944	46.30	25	 	+	10.5	SPLT	5.40	N/L	 		117	214	1	1	1	t	1	1			· · · · ·								
198	32861	80944	46.30	2.5	 	+	10.5	+ SPLT	4,40	I ML			<u> </u>	+ <u>*!</u>	<u>t</u>	<u> </u>	1	<u> </u>	<u> </u>	<u> </u>			[·						CBC Gym., Wakefield St.		
199	32172	81587	49.80	1.1			>3.0		+	+		+	<u> </u>		1	t	† – – – – – – – – – – – – – – – – – – –	<u> </u>		1					T				Botanic Park Conservatory	l	
1 200							-				-		-	-		-	-	-	-	-	-						_				

Table C.3Data from SACON

Ref. Na.	AMG Nerth.	Coords. East.	Surface RL (m) (AED)	Depth to Kerwick	Top of L Sand	.ayer (m) Lower	Depth to Botiom of Layer (m)	Test Type	Test Depth (m)	Soll Layer Tested	Undrained Shear Strength su (kPa)	Confining Prussure (kPa)	Undrained Young's Medules (MPa)	Undrained Shear Strength cs (kPs)	Internal Angle of Priction (degrees)	Dry Density (#m3)	Dry Unit Wolght (kN/m3)	Water Content (%)	Total Suction (pF)	Bulk Unk Weight (kNim3)	Void Ratio	Degree of Saturation (%)	Back- Calculated Specific Gravity	Cooff. of Earth Prossure at Rost	instab- iliy Index (%)	SPT Dapth (m)	Deta N	Season/ Year	Location	Comments	Assumed Constants and Legand
	E	hata Sourc				SACON	160		T1			· · · · ·		-							<u> </u>								Gov. Office Building		Specific
201	32027	80570	44.00	24	1.9	<u>9,7</u> 11.2	13.8																						Victoria Sq. West		Oravity,
203	31982	80575	44.20	21	8.9	10.4	14.0																								G = 27
204	31900	80552	44.20	2.2	8,6	10.2	13.9		-							1 417	14.10	917		18 57	0.88	97.38		-		10.2	37	W/1970	Western Courts Building		<u>e</u> r
205	31810	80589	44.80	1.2	9.1	11.4	15.0	TCUI	2.85	ĸ	179	148				1.424	13.97	32.7		18.54	0.90	98.53							MEE SL		
205	31810	80589	44,80	1.2	9.1	11.4	15.0	TCUI	4.65	K	102	88				1.397	13.70	32.9		18.21	9.93	95.24						1			
205	31810	80589	44.80	1.2	9.1	11.4	15.0	TCUI	4.65	K.	110	189				1.383	13.57	36.0		18.45	0.95	102.07	2.75								
205	31810	80589	44.80	1.2	9.1	11.4	15.0	TCUI	9.75	<u> </u>	310	179				1.405	13.78	33.2		18.07	0.04	47.25				10,1	31	W/1970			
206	31846	80569	44.60	22	8.0	10.6	14.6	TCUI	2.85	ĸ	50	55				1.386	13.60	33.9		18.21	0.95	96.55									Test Types:
206	31846	80569	44.60	2.2	8.6	10.6	14.6	TCUI	6.25	ĸ	119	117				1.379	13.53	34.7		16.22	0.96	97,80									SPLT = Screw Plate
206	31846	80569	44.60	2.2	8.6	10.6	14.6	TCUI	6.25	K	110	235				1.371	13.45	35.4	┝──┥	18.21	0.97	21.60									Loss Ten. SBPT - Salf Barine
206	31846	80569	44.60	22	8.6	10.6	14.6	TCUI	10.90		347	232				1.559	15.29	254	┝──┼	10 12	0.01	93.70									Prostantine Tool.
200	31840	8/17.48	44.60	28	8.0	11.5	18.3	TUU3	3.18	x X	\$0	55	19.5	65	5.6	1.46	14.32	30.7								19.7	>50	\$/1976,7	Catholic Precinct Towar		CPT = Caus Penetration
											84	138																	Walasfield SL		Test.
											103	276							┨┤												TUUF = Triaxial, Uncommissional Understand
207	31993	80748	45.00	2.8	9.9	11.5	18.3	TUU3	4.67	K.	96	83	24.5	<u> </u>	0.5	1.39	13.64	32.0		18.41	0.94	100.27	4./1								test with # staget.
\vdash									+		100	345									-										TCD# = Triazial,
207	31993	80748	45.00	2.8	9.9	11.5	18.3	TUU3	7.73	ĸ	159	134	31.8	151	1.7	1,43	14.03	32.9		18.64	0.89	100.02	2.70								Coussilidated, Drained
											165	276							┠────┤												TEN Trianial
						<u> </u>			+ <u></u>		172	552		102	1.2	14	16.00	21.4	┠──┤	10 4<	0.44	97.75									Unconfined Community
207	31993	80748	45.00	2.8	9.9	11.5	18.3	1003	12.29	-	202	414	<u> 20.4</u>	541 241		1.04	10.07	<u></u>		17.01											Test.
\square			<u> </u>				<u> </u> †				216	827																			DST = Direct Shear Test.
207	31993	80748	45.00	2.8	9.9	11.5	18.3	TUU2	16.87	L.	484	310	48.3	456	. 21	1.76	17.27	19.2	↓ Ţ	20.58	0.53	97.06			-		<u> </u>				
		_							<u> </u>		496	621	10.0		16		14.12	31 *	┟╍╍╍┝	18 67	0.88	98.11						\$/1976.7			S - Summer
208	32053	80770	45.00	1.5	8.7	10.7	17.1	TUU3	1.64	ĸ	78	<u>28</u> 60	12.9		3.0	-193-	-19.13	31.4		19.04		- 20.13						347221021			A = Autumn
											85	138																			W = Winter
208	32053	80770	45.00	1.5	8.7	10.7	17.1	TUUS	3.18	X	58	55	19.3	55	2.1	1,37	13.44	36.0		18.28	0.97	100.12	2.70								Sp = Spring
											63	138		<u> </u>																	
			47.00			10.2		711112	40		66	276	201	148	1.3	1.4	13.73	34.6		18.49	0.93	100.61	2.72								
2.6	3003	80770	45.00	- 13		19.7	17.1	1003	9.07	•	156	207																			
											160	414																			
206	32053	80770	45.00	1.5	8.7	10.7	17.1	TUU3	10.78	L	676	193	67.8	616	4.3	1,82	17.85	17.4		20.96	0.48	97.16	.								
				 				· ·			704	414				·					-										
208	32053	80770	45.00	1.5	\$7	10.7	17.1	TUU2	16.90	L	366	324	24.4	353	1.1	1,79	17.56	17.8		20.69	0.51	94.54									
											373	689																		i	<u></u>
209	32101	80644	45.80	3.7			18.3	TUU3	4.87	K/L			26	110	5	1.58	15.50	25.9		19.51	0.71	98.65			↓			Sp/1977	Wakafinid House, 30 Wakafinid St.		<u></u>
209	32101	80644	45.80	3.7			18.3	TUU3	6.39	KA.			44	100	3	1.47	14.13	32.0		18.65	0.85	98.74									
209	32101	30844	45.80	3.7			18.3	TUU3	9.29	KAL			52	200	3	1.66	16.28	22.3		19.92	0.63	96.10									
209	32101	80844	45.80	3.7			18.3	TUU3	12.33	K/L.			40	265	1	1.51	14.81	28.3	[19.01	0.79	96.96									
209	32101	80644	45.80	3.7			18.3	TUU3	15.37	K/L		ļ	34	170	<u> </u>	1.48	14.52	30.6		18.96	0.82	100.23	2.71								
209	32101	80844	45.80	3.7			18.3	TUU3	16.89	KA.		<u> </u>	40	295	0	1.2	13.83	33.8		19.14	0.00	99.75	- 6/3			_		Sp/1977			
210	32098	30805	45.80	2.8	10.3	121	15.7	TUU3	6.24	ĸ			32	140	1	1.43	14.03	32.1		18.53	0.89	97.59	_					•			
210	32098	80806	45.80	2.8	10.3	12.1	15.7	TUU3	7.76	K			36	175	1	1.43	14.03	31.5		18,45	0.89	95.76									
210	32098	80806	45.80	2.8	10.3	12.1	15.7	TUU3	9.29	K		 	40	215	-	1.42	13.93	32.0		18.39	0.90										
210	32098	80606	45.80	2.8	10.3	12.1	15.7	TUU3	15.37	L.			10	45	3	1.43	14.03	32.5	<u> </u>	18.59	0.19	98.81						Sp/1977			
211	32124	80806	45.80	2.6	9.6	11.1	15.5	TUU3	6.24	x		<u> </u>	28	135	1	1.48	14.52	30,2		18.90	0.82	98.92									
211	32124	80806	45,80	2.6	9.6	11.1	15.5	TUU3	7.76	ĸ		[40	195	1	1.44	14.13	32.2		18.68	0.88	99.36									
211	32124	80806	45.80	2.6	9.6	.11.1	15.5	TUU3	9.29	ĸ			40	195	2	1.47	14.42	29.7	 	18.70	0.84	95.84			┝						
211	32124	80806	45.80	2.6	9.6	11.1	15.5	TUU3	12.33	<u>-</u>		 	<u>61</u>	370	<u> </u>	1.75	17.17	30.6		18 32	0.24	93.03									
211	32124	80806	45.80	2.6	9.6	11.1	13.5	1003	13.37	r K		<u></u>	36	175	1	1.58	15.50	25.9		19.51	0.71	98.65						Sp/1977			
212	32118	80842	45.80	3.3	11.7	12.7	19.0	TUU3	6.24	ĸ			30	175	3	1.51	14.81	28.7		19.06	0.79	98.33									
212	32118	80842	45.80	3.3	11.7	12.7	19.0	TUU3	7.76	ĸ		1	24	145	4	1.46	14.32	31.0	 	18.76	0.85	98.55			┟╼╼╾┥		\vdash				
212	32118	80842	45.80	3.3	11.7	12.7	19.0	TUU3	9.29	<u>K</u>		 	24	140	<u> </u>	1.42	13.93	321	 	20 12	0.90				┝╼╼┥						
212	32118	80842	45.80	3.3	11.7	12.7	19.0	TUU3	12.33	5		<u> </u>	21	245	4	1.64	16.09	23.6		19.89	0.65	98.59						ļ			
212	32118	80642	45.80	3.3	11.7	127	19.0	TUU3	17.09	ī	<u> </u>	<u> </u>	40	145	5	1.45	14.22	31.1		18.65	0.86	97.41									
212	32118	80842	45.80	3.3	11.7	12.7	19.0	TUU3	18.43	L			30	100	1	1.38	13.54	34.7	<u> </u>	18.24	0.96	97,95			┝──┤			1077	Barrada Sair		
			 			Į		TCU3	5.85	X/L	108	112		├ ────		1.51	14.81	28.6	┼───	19.05	0.79	<u>. 97.99</u>			<u> </u>		-	19/3	A Motor Vehicles Dent.		
			+				┨───┤		-		240	664	<u> </u>	<u> </u>	 			L										1			
			1					TCU2	7.80	KA.	167	148				1,50	14.72	29.6		19.07	0.80	99.90						i			
			L								183	483	1	1					 						┟╼╾┥						
			<u> </u>	I	<u> </u>]	TCU2	7.80	KAL	170	389	<u> </u>	<u>+</u>		1.47	14,42	30.6	┼	18.83	0.84	98.74			┟╍╍╍┥			i			
	├ ──┤	├	1				┼──┤	TITIT	0.75	XA.	196	170	<u> </u>			1.41	13.83	33.3		18.44	0.91	98.27						1			
\vdash			<u> </u>		 	<u> </u>	<u> </u> −−−−	1002	1	~/L	207	572																			
			1					TCU3	11.70	K/L	191	230				1.57	15.40	25.4	<u> </u>	19.31	0.72	95.28									
			1	1					1		229	614	ļ	 	 			ŀ							┼───┤						
		ļ	╉────				↓↓	TANIA	111 70	¥#	251	<u>862</u> (34			<u> </u>	1.61	15.79	24.0	+	19.58	0.68	95.71									
			1			<u> </u>	<u> </u>	1002	11.70	- N/L	289	\$62	L	<u> </u>																	
								TCU2	3.50	KA.	99	64				1.40	13.73	32.7	↓	18.23	0.93	95.08		ļ	┟╾╌╴╴╴						
				1							124	269	ļ	ļ	ļ		19.44	+	╂────-						┟┅╾─┤		<u> </u>				
			1	1	1		1 1	0.000	1 2 50	1 164	1 103	1 106	1	1		1 1.39	13.95	1 33.8	1	18.24	0.94	96.83									

	AMG	Canada	-	Danib t	a Tan of I		Danih ia	1	1	1 Sell	These	Confining	Underland	Undrained	Internal	Dry	Dre	Water	Total	Bulk		Degree	Beck-	Ceeff.	Instab-	178	Deta				
Ref.			RL		1		Bottom	Test	Test	Layer	Shear	Pressure	Young's	Shear	Angle of	Density	Unit	Content	Suction	Unit	Void	4	Coloulated	of Barth	iii y	Depth		Seese.	Location	Comments	Assumed Constants
Ne.	North.	East.	(m)	Kerwici	Sand	Lower	of Layer	Туре	Depti	Tested	Strength	(kiPa)	Modulus	Strength	Friction	(Vm3)	Weight	(%)	(P P)	Weight	Ratio	Saturation	Specific	Pressere	Index	(11)	N	Year			and Legend
			(AHD)				(m)				su (kPa)		(MPn)	cu (kPa)	(degraes)	1	(kN/m3)	L		(M/m3)		_(%)	GREET	l al Kest	(%)	L					
	D	nia Sourc	e t	Wei	dbern Fil	<u>phardine</u>	e Geoteci	haical		T	1					1	r				1 1								Cur Genear St & Ment Lana		Specific
213	31842	79651	40.60	2.2			>11.0	╉	-	-	<u> </u>				<u> </u>		<u> </u>												Art Gellery, North Tee.		Oravity.
219	33044	81001	40.20	20	+	<u> </u>	8.0					t																			G=
216	32986	80985	42.70	1.5		6.6	9.1			1																					2.7
217	32627	80536	43.90	1.5			11.4																						Gilbert FL		
218	32622	80560	44.50	1.9			12.9																	ļ							
219	32166	81394	48.60	3.2	11.3	13.6	>19.6		-			ļ			ļ	ļ													Cor. Waitefield & Prome Sta.		
220	32064	\$1170	47.50	3.0			>5.0	ļ	_							 									-				131 WARDING 3L		Test Types:
221	32410	\$1570	41.20	3.0	· ··	9.7	14.0	<u> </u>	+	+		<u> </u>																	75-89 Gunfull St		SPLT = Screw Plate
777	32472	PU091	45,40	20			13.1			1		 																			Losd Test.
224	31753	80547	44.60	15			17.8	1	-	+			·					-											34-48 Wright St.		SBPT - Solf Boring
225	32697	80668	43.88	2.0	9.5	11.6	15.2			1	1																		Myur/REMM Development		Programmeter Test.
226	32817	80657	42.64	2.4			11.7																		l	L					CPT = Come Penetration
				1.5	10.8	11.8	15.0		2.20	ĸ					L						<u> </u>			 	3.3	11.0	27	W/1967		Core Shrinkage Method	Test.
				1.5	10.8	11.8	15.0		4.00	K			 	L	 	Į					╉╌╌┥			<u> </u>	5.4		~				TUUW = Thiazial,
227	32701	80731	44.50	1.7	10.7	11.3	14,4		+				 							18 20		87 68				11.9	4/	Wneer			ing with a state
228	32722	80749	44,50	1.2	 		8.2	<u>1 TUU2</u>	+ 3.25	KAL		70	 	<u>80</u>		1-1.39	13,64	34,7	-2.00	19.30	+****	- 21.22						.,			TCD# = Triazial.
	30700		44.50		╉			ł	1 4 40	1 10	 " -	- 200				t						I			4.6						Consolidated, Drained
224	34/44	80749	44.30	1.6			8.4	71113	415	KA.	90	130	1		l	1.49	14.52	29.7	4.18	18.83	0.82	97.28									test with # stages.
1.000					1			1 1000		1	115	380																			TUC = Triazial,
		···			1				-		115	630																			Unconfined Compression
228	32722	80749	44.50	1.2			8.2		7.50	K/L															2.2						Test
229	32842	\$0701	43.40	1.7			9.8	TUU3	2.05	KL	160	40	L	160	0	1.44	14,13	31.7	3.83	18.60	0.88	97.82						W/1987			DST = Direct Shear Test.
									_	<u> </u>	150	120				 					+										
				[-		160	200							416	18.67	0.01	101.20	2.78								Sanana ti
.229	32842	80701	43,40	1.7			9.8	<u>TUU3</u>	5.15	KAL	115	102		112	<u> </u>	1 1.41	13.83	33.0	4.10	16.0/		103.29	~/.								S = Summer
				<u> </u>						+	115	500				<u> </u>															A - Automa
220	37847	80701	43.40	17			0.2	TINK	6.65	KA.	185	140		175	1	1.44	14.13	33.4	4.21	18.84	0.88	103.06	2.77								W = Winter
							- /			1	185	420																			Sp = Spring
										1	190	700																			
230	32738	80656	44.10	1.3			12.2	TUU3	1.65	K/L	36	40		32	2	1.29	12.65	40.6	3.35	17.79	1.09	100.29	2,7]		 			W/1987		· · · · · · · · · · · · · · · · · · ·	
											37	114									├ 										· · · · · · · · · · · · · · · · · · ·
									-		38	190					16.01		2.03	10.12	676	M6 74									
230	32738	80656	44.10	1.3			122		4.65	KAL	155	100		152	- - -	1.23	10.01	31.4	3.22	12.16	0.70	74./4									
\vdash	├──┨							1	+	1-	152	440					<u> </u>														
230	32738	80656	44.10	1.3			12.2	TUUS	7.65	KA.	180	160	 	175	0	1.73	16.97		4.23		0.56										
				<u> </u>	1						175	480														_					
									1		175	790																			
230	32738	80656	44.10	1.3			12.2	TUUS	10.65	KA.	120	220		105	2	1.39	13.64	36.0	3.86	18.54	0.94	103.14	2.78			┝──┤					
								+	4	1	145	660									+			<u> </u>							
				 					+	+	145	1160	 		 		1 14 14			20.07	64	101 83	2.73					W/1074	Adeleide Submey Stude		····
231	35020	80407	50.00	26	4.8	5.3	13.8		4.06	<u> </u>	310		 	310		1.63	14 12	310		18 76	0.85	98.55							······································		
201	35020	20407	50.00	20	1.0	3.3	12.0		2.90		170		 	179		1.30	13.64	35.0		18.41	0.94	100.27	2.71								
211	35020	80407	50.00	2.6	4.8	5.3	13.8	TUC	10.15	i L	310	6	İ	310		1.49	14.62	30.0		19.00	0.81	99,74									
231	35020	80407	50.00	2.6	4.8	5.3	13.8	TUC	12.33	Πī	317	Ō	ľ	317		1.49	14.62	27.0		18.56	0.81	89.77									
232	34798	81578	34.30	NÆ									[· · · · ·						
233	33696	81654	31.10	NA																											
234	33515	80759	28.00	N/E																	_										
235	33519	79458	24.00	N/B					4	1	 	 	I		ļ	 	 				+										
236	33933	79376	36.80	23	I		6.9	 	+	1	 	 	I		 	<u> </u>					┝──┤					 					
237	34257	80677	45.20	1.3	┟╍┈╍┥		6.2		+			<u> </u>	 		<u> </u>	<u> </u>	<u> </u>				┝──┤										
238	34468	81084	32.20	N/E			100		+	+		<u> </u>	<u> </u>			<u>├</u>					 					1					

Table C.4 Data from Golder Associates Pty. Ltd. (formerly Woodburn Fitzhardinge Geotechnical).

														1			0	Watan	Tetal	P. B	-	Denne	Back	Coeff.	I mainte	SPT	Deta			I	
	AMG_	Coords.	Surface	Depth to	Top of I	Lever (m)	Depth to			5-8	Undrained	Confining	Undrained	Undrained	Internal	Dry	Ury	Content	Local .	i inter	1		Coloubiad	of Rarth	N ity	Depth		Seeres/	Location	Commonis	Assumed Constants
Ref.			RL.				Bottem	Test	Test	Layer	Speer	Pressure	Toung's	Same?	Anger of	14-30	W.L.L	(6)	(13)	Walahi	Ratio	Sector Sector	Smelle	Pressure	lader	(=)	N	Year			and Legend
Ne.	North.	Bast.	(=)	Kerwich	Sand	Lower	of Layer	Type	Depth	Tested	Strongth	(8279)	() (The)	aurungun	(desmark	(*=.5)	(InN/mit)	(**)	()	(kNim3)		(16)	Gravity	at Rest	(5)						
			(AHD)	<u> </u>	<u> </u>			<u> </u>	(1)	<u> </u>					البند ددال					(2000)											
		Data Sourc	#	He	nsking Ol T	bern Free	nan sad 1	TOR	Tree		1 100	1 107	(1)	190	14	1.44	14.13	30.5		18.43	0.85	94.11						W/1977	Anthor St., Nth. Ad.		Specific
240	34474	80137	47.80	5.7			>6.39	1003	6.22		100	10/	74-6																		Gravity,
		L			 					+	- 11/	314				{		_													G=
								 			1 197	42/		130	-	1.0	14.01	28.0		18.08	0.78	67.34						W/1977			2.7
241	34453	\$0070	47.10	5.6			>6.44	<u>TUU3</u>	6.28	L KL	204	10/	42.2	<u> </u>		<u> </u>	-19-21	60.V		17.47											
					ļ			ļ			215	214	<u> </u>																		
					 				+	1	246	42/			\vdash	1 14	14.99	20.5	3.46	18 44	0.85	83.78						W/1977			
242	34435	80016	46.70	4.0			9.5	TUU3	6.25	KL	122	107	29.4	110	<u>⊢ , </u>	146	17.24			10.33		73.78									
			<u> </u>						4		129	214		<u>}</u>										1							
										+	141	42/			<u> </u>	1.46	14.12	28.0		19 77	0.95	99.01									Test Types:
242	34435	\$0016	46.70	4.0			9.5	TUU3	7,78		61	138	20./	- 26-	┝╌┛╌	100	-19.24			19.22											SPLT = Screw Plats
								<u> </u>	+		- 73	2/0				1															Load Test.
					I				1	+	85		10.1	196		1 17	13.44	35.0	3.83	18.14	0.97	67.34						W/1977			SBPT = Soif Boring
243	34421	80210	47.70	4.0	<u> </u>		10.0	TUU3	5.80		100	105	- 1041		•,-	1.07	19171			10,14	~ /-										Preasuremeter Test.
					ļ	_					190	201		<u> </u>																	CPT = Cone Penetration
				<u> </u>	├ ──				+	1	217	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	36.7	175	0 <	1.5	14.72	28.5		18.01	0.00	96.19									Teel
243	34421	80210	47.70	4.0	 	+	10.0	1003	17.72	1.44	+ 177	1.28	- <u></u>	t-""		1-11					1								l		TUU# = Triazial,
				<u> </u>						+		610	<u> </u>			1										T					Unconsolidated, Undrained
					 				1				42.2	180	<	1 47	14.42	30.0		18.75	0 24	96.80						W/1977			wat with # stages.
244	34394	80158	47,00	3.7			7.0	1003	1 012	- ML	240	214	43.3		<u> </u>	<u> </u>											·				TCD# = Triazial,
				ļ	ļ	<u> </u>	 			+	- 205	414	 																		Consolidated, Drained
	· · · ·								1 1 1		240	46/	361	120	4	14	13.73	33.5		18 33	0.93	97.41									test with # stages.
245	34377	80107	46.70	3.1	<u> </u>		<u></u>	1 1003	6.25	M	13/	100	- 20.1							Lette											TUC = Triaxial,
		·····		I		+		<u> </u>	+	+	1.140	419		1		t															Unconfined Compression
									1 0.00	-	102	961	17.0															W/1982	Suns Aquatic Contro, Hindley St.		Test.
246	32578	79713	39.70	2.0			6.0	SPLT	2.00	N/L	+		40.0	07	<u> </u>									1					•		DST = Direct Shear Test.
246	32578	79713	39.70	2.0			6.0	SPLT	4.00	K/L	<u> </u>			12		<u> </u>		31.5	4.03												
246	32578	79713	39.70	2.0			0.0	100	4.03				87.0			<u>† </u>					1										
246	32578	79713	39.70	2.0	<u> </u>		0.0	SPLI	0.00				28.0	81														W/1982			Sensons:
247	3250	79733	39.20	20	<u> </u>		3.3	3611	2.00	W.L.				65	0	1		32.3	3.91		1					_					S = Summer
247	3236	19155	39.00	20	+	+	3.3	100	4.00	NA.	<u> </u>		37.0	103																	A = Autuma
24/	3/24	79/33	37.60	<u> </u>			5.5	epr T	2.00	WA.	1		36.0	91		1												W/1982			W = Winter
248	32222	79751	39.00		+	+	5.0	EDI T	4.00	KA			57.0	141																	Sp = Spring
249	32532	79731	30.00	14	+	+	5.6	SPLT	2.00	XA.			36.0	117																	·····
250	32540	81254	44 50	17		+	>10.7	TIAR	3.18	XA.	125	55	7.9	135	0	1.369	13.43	35.8	3.83	18.24	0.97	99.42						A/1979	Academy Cinemas, Hindusch Sq.		
100	3407/		1	+ **	1			1			130	110																			
	<u> </u>	<u> </u>	1	1	1	1	<u> </u>	1	1	1	137	221	T																		
250	32607	81254	44 50	3.7	1	1	>10.7	TUU3	5.20	KA.	138	89	10.5	140	1.1	1.454	14.26	31.8	4.17	18.80	0.86	100,19	2.70			↓ ↓					
	1	1	1	1	1			1			150	179											· ·	↓				1			
	<u> </u>	1	1	<u> </u>	1		1				166	359						L			1			<u> </u>		 		1			
250	32647	81254	44.50	3.7	1	1	>10.7	TUU3	7.20	KA.	123	128	14.7	117	1.7	1.421	13.94	33.2		18.57	0.90	99.59		<u> </u>		 					·*
		1	1		1		1				141	255			1	1									<u> </u>						
						1					168	510														ļ					
251	32669	\$1232	43.90	3.0			>6.3	TUU3	3.06	KAL	229	48		245	0.8	1,406	13.81	33.1	4.04	18.38	0.92	97.39	L	l	 	┝──┥		A/19/9			
			T								235	97		L							_					┝╌╼┥		1			
							1	1			247	193		L		<u> </u>			<u> </u>		I					<u> </u>		ł			······
251	32669	\$1232	43.90	3.0			>6.3	TUU2	4.65	KA	140	79	18.0	146	1.2	1.409	13.82	33.2	4.15	18.41	0.92	97.83	<u> </u>	<u> </u>		┣━━━┫		{		<u> </u>	
		1	1								148	159			L	L					<u> </u>		<u> </u>	1	┞───			ł	c.		
251	32669	\$1232	43.90	3.0			>6.3	TUU3	6.07	KA.	177	107	18.0	184	0	1.469	14.41	30.3	4.25	18.78	0.84	97.63	 	 	 	ļ		1			······
			1	1							186	214			I	J			L			L	L		<u> </u>			4			
—	1			1	1	1	Ι				203	427			L	L			 			L	L	ļ	 	<u> </u>		 			·
252	32635	\$1252	45.00	2.7			>10.7	TUU2	5.20	KA	149	93	20.0	138	2.6	1.41	13,83	33.2	4.17	18.42	0.91	97.98	L			┟╌╍┥		1			
								1			162	186	L		<u> </u>	<u> </u>	L		<u> </u>					+	— ~	┣━━━┥		1			
252	32635	\$1252	45.00	2.7			>10.7	TUU2	7.20	KA.	162	131	14.0	167	0.1	1.44	14.13	31.9		18.63	0.88	98.43	 	+	ļ	-		1			
	1	1	1	1	1		1	1			172	262	1		1	1	1		1	1	1	ł	I	I	1	1	l	I		· · · · · · · · · · · · · · · · · · ·	

Table C.5Data from ACER Wargon Chapman Pty. Ltd. (formerly Hosking Oborn Freeman and Fox).

Table C.6Data from Koukourou and Partners.

											1	Candinana	أفيساعها	Inderstand	Internal	Der	De-	Water	Tetal	Br B		Denes	Back.	Conff.	Instab-	SPT	Deta	1			
	AMC	Ceerds.	Surface	Depth to	Top of L	.əyer (m)	Depth to Bottom	Tori		Javer	Sheer I	Pressure	Young's	Sheer	Angle of	Density	Unit	Content	Suction	Unit	Vold	4	Calculated	of Barth	illity	Depth		Seesen/	Location	Comments	Assumed Constants
No.	North.	East.	(Kerwick	Sand	Lower	of Layer	Type	Depth	Tested	Strength	(kPa)	Modulus	Strength	Friction	(#m3)	Weight	(%)	(HP)	Weight	Ratio	Saturation	Specific	Pressure	Index	(m)	N	Ymr			and Legend
		L	(AHD)			1	(m)	L	<u>(m)</u>		en (kPa)		(1407%)	gu (kPa)	(degrees)		(<u>kN/m3)</u>			(kN/m3)		(19)	Granity		(79)		1			LL	
L	<u>1</u>	Data Searc			Koskos	ree and I	Artaers	79.1123	No.1	¥#		60	18	95	0.3	1.4	13.73	34.2	·)	18.43	0.93	99.44						S/1983	Car. West Tos & Waymouth St.		Specific
253	32314	79557	40.50	2.5			>/,0	1003	3.65			138																			Oravity,
-												276																			0 • 27
254	32348	79580	40.50	3.9			>7.0	TUU3	5.15	K/L			22	110	0,4	145	14.22	31.6		18.72	0.86	<u>_98.97</u>						S/1983			6 1
												193																			
			ļ									386				147	14.42	30.8		18.86	0.84	99,39						\$/1983			
255	32312	79579	40.70	2.7			>1.0	<u>TUU3</u>	3.65	M I		<u>69</u>		76	<u></u>	-191-															
												276																			
256	31265	80324	42.20	4.2			13.7	TUU3	6.25	KI	119	120	16	120	0	1.41	13.83	34,2		18.56	9.91	100.93	2.72					W/1984	99-102 South Tcs.		Test Types:
1	2100										110	240													<u> </u>						Set. 1 = Screw Field
									<u> </u>		105	480					14.70	20.4		10.00	0.00	A5 85			┣────			W/1964			SEPT - Self Boring
256	31265	80324	42.20	4.2			13.7	TUU3	12.35	KA.	176	238	15	1/9		-1-2	-19.76			10.07		- 1141						.,			Programmer Test.
											1/2	4/0			_																CPT = Cons Penetration
1 257	31779	80122	42 30	- 16			14.5	TUU3	6.75	KA.	131	131	18	127	1.6	1.39	13.64	35.1		18.42	0.94	100.56	2.71					W/1964			Test
	216/2			- 210							144	262													I						TUDS = TRAXIAL,
											144	524																			that with f stand.
257	31279	\$0322	42.30	3.6		ļ	14.5	SPLT	6.30	KA.			63	115											<u> </u>						TCD# = Triazial,
257	31279	\$0322	42.30	3.6			14.5	SPLT	9.30	KAL		107	32	209	0	1.455	14.27	32.2		18.87	0.86	101.60	2.74					W/1984			Consoliaded, Drained
257	31279	80322	42.30	3.6			14.3	1003	9.93		207	386				1.12-															test with # stages.
	<u> </u>	<u> </u>	+			<u> </u>			1		202	772												ļ	<u> </u>	\vdash					TUC = Triaxial,
258	32780	80411	32.95	NÆ															├ ──-	<u> </u>	┝			ļ	ł	\vdash		0	STA Building, North Tcs.	1	URCOMMENT COMPRESSION
259	32778	80390	36.60	4.3			>5.6	SPLT	4.57	K/L			70	151					├ ──	18.53		85.877			 	┝──┤		3p/1984			DST - Direct Shear Test
259	32778	80390	36.60	4.3		ļ	>5.6	TUU3	5.15	KA.	104	103	18	104	0.3	1.44	14,13	21.1		18.52	0.88	. 19.97		i —							
		ļ	<u> </u>	 		 		├ ────	╂───	<u>├</u>	106	207										ł									
				NE		∤	212.2		t	┟──┤	100	-14																	SAIT Bosython Building		Sensons:
260	33119	79238	31.00	27		╂────	>10.7	TUU3	3.15	KA.	101	55	30	92	0	1.4	13.73	34,2		18.43	0.93	99.44						S/1986	2 & 3 Greenhill R.d., Wayville		S = Summer
		1	1 3								106	110																			A = AUGUER
			1								114	220													 			\$11086			Sn = Spring
261	30466	79238	31.00	2.7			>10.7	TUU3	4.75	K/L	<u>97</u>	83	29	83	1.5	1.44	14.13	32.2	<u> </u>	18.68	0.88	99.30			<u> </u>			3/1940			
_		L	<u> </u>			╂────			 		109	165																			
		-	33.40	NE		├ ──	>26.5	·	+			331	<u> </u>																SAIT Nursing Building		
262	33030	81230	48 50	26		1	>14.1	TUU3	4.65	KA.	91	103	27	77	1.3	1.38	13.54	35,4		18.33	0.96	99.92		ļ				A/1987	Car. Hutt & Plinders Sts.		
100	34670	01/10	1			1					104	207												.							
											128	414																			
263	32298	\$1716	48.50	26	<u> </u>	<u> </u>	>14.1	TUU3	7.75	K/L	310	136	36	259	3.7	1.63	17.95	10.9		20.99	0.48	92.94									
	·	I		ļ					-		334	<u>7/6</u>	<u> </u>												1						
-	20000	01716	49.50	- 26			5141	771113	10.85	¥A.	303	172	58	274	4.2	1.84	18.05	17.3		21.17	0.47	99.94									
200	24454	e 1/10	40.30	- <u></u>		1		1003	10.05	- 24.5	373	345													L						
-	1		1	1							420	_ 690																	Only that Designed Transm	CTT T unbusy may not be approved	
208	32053	80770	45.00	2.6			>14.1	SPLT	2.75	K/L		<u> </u>	69	190										}				5/19//,8	Campara Prochet Town	STLI VANAS MAI NOT DE GAUGE	
208	32053	80770	45.00	2.6	ļ		>14.1	SPLT	3.34	KA.		ļ	91	250										<u> </u>	<u> </u>						
208	32053	80770	45.00	2.6	<u> </u>		>14.1	SPLT	4.00	KA.		·	50	225																	
208	32053	80770	45.00	20			14.5		4.95	KA.	179	86	75	178	0	1.44	14.13	31.0		18.51	0.88	95.66						S/1961	Telecom Building, Pine St.		
403.	32430		43.20	- 23			- 19.5	1003	1 3.00		178	172													ļ						
	1		1			1	_				180	345				-			$ \longrightarrow $						<u> </u>						
263.	32430	80718	45.20	2.3			14.5	TUU3	6.25	KL	179	110	36.5	159	5	1.42	13.93	32.0	—	18.39	0.90	95.85			<u> </u>						
		1	1		ļ	1		ļ	1	 	202	221	├ ───						├ ───		+-+			<u> </u>	 	┝─┤					
	<u> </u>		+	<u> </u>	 		ļ	-	+		214	441	<u> </u>	140	-	1 44	14 12	31.0	+	18 76	0.85	98.55		t	t						
263.	32430	80718	45.20	23	<u> </u>		14.5	<u>UU3_</u>	7.75	KL	178	276		100		1.40			<u> </u>												
H-		 	+	<u> </u>	<u> </u>	1	 	1	+	1	191	552	1																		
261	32430	80715	45,20	23	t	1	14.5	TUU3	9.35	KA.	293	165	49	282	1	1.49	14.62	30.0	ļ	19.00	0,81	99.74		 	ļ	└──┤					
	1										298	331						 	 	ļ			<u> </u>	 	<u> </u>	┝──┦					
	1		1					L	1		305	662	 			1 40	14.62	20.0	╉╼╍──┤	10 00	1 I	00.74		├ ───	<u> </u>	┟──┤				t	
263.	32430	80718	45.20	23	 	.l	14.5	TUUI	10.85	K/L	330	190		330	2	1.49	13 83	34.0	+	18 54	0.01	100.34	2.71		1	├──-┦					
263.	32430	80718	45.20	2.3		+	14.5	1003	12.35	I ML.	209	414		170	· · · · ·																
\vdash	┫~───		+	1		+	<u> </u>	╂─────	+		236	\$62	1												I						
261	32430	80718	45.20	2.3		1	14.5	TUU3	13.85	KAL	284	241	45	. 241	2	1.39	13.64	34.0	ļ	18.27	0.94	97.41	ļ	ļ	 	┟───┥				<u> </u>	
											275	483	1	ļ			 		 		\square		<u> </u>	<u> </u>	├ ──	┞──┦					
										+	285	862	+	<u> </u>			I	<u> </u>	 		+				+	┝╌─┤		5/1981			
264	32408	\$0766	45.50	1.6	<u> </u>	+	15.2	SPLT	4.50	KAL			-	127	+ .	1 40	14.42	20.0	+	18.84	0.81	96.42	——	1	1	┟──┨					
264	32408	80766	45.50	1.6	<u> </u>	+	15.2	TUU3_	4.95	KA.	164	172	<u>+∞</u>	<u> </u>	t • •		1														
	+	1	+	+	 	+	<u> </u>		1-		168	345	1	1			[
264	32400	8/1764	45.50	16	├	1	15.2	TUU3	6.25	KA.	183	110	33	169	3	1.47	14.42	30.0		18.75	0.84	96.80			1					ļ	
	1-20-00	1		1	1	1			1		191	221						ļ	4				ļ	ļ	 	├					
	1				L						201	441	1		Į		Į	I	- 	— —				┨	╂────	┝──┤					
264	32408	80766	45.50	1.6			15.2	SPLT	6.10	K/L	ļ	<u> </u>	36	109	 		ł	<u> </u>	+				├	<u> </u>	<u> </u>	┝╶╌╴┨					
264	32408	80766	45.50	1.6	I		15.2	SPLT	7.60	KAL.		<u> </u>	42	138	<u>├</u> ,	1.45	14.22	110	+	18.63	0.86	97.09	<u> </u>	1							
264	32408	80766	45.50	1.6	├──	-	15.2	TUU3	1.75	KAL.	217	774	+ <u>//</u>	- <u>410</u>	<u>-</u>	1.72		1													
-	+	 		<u> </u>	<u> </u>	+	 —	+	+	1	225	552	<u>+</u>	1																	
264	37408	80764	45 50	1.6	1	+	152	TUIN	9.35	KA	179	165	102	176	1	1.46	14.32	31.0	1	18.76	0.85	98.55		L	<u> </u>]				·····	
1	1-10-10-	00700		1	1	1	1				180	331						1	+	L				 	╂───	+					
											182	662	<u> </u>	<u> </u>	 	┞────	<u> </u>			 				 	 						
264	32408	80766	45.50	1.6	<u> </u>	4	15.2	SPLT	9.20	KAL	 	┟	26	220		┣───	1	<u> </u>	+		├ ──┤		<u> </u>	+	<u> </u>	11					
264	32408	80766	45.50	1.6	 	+	15.2	SPLT	10.70	NAL NAL	110	1.00	43	179		1.46	14.32	31.0	+	18.76	0.85	98.55	<u> </u>		1	tt					
1 344	1	1 40044	1 46 60																-			79.33	-		·						

	AMG	Ceerd	Surfa RI.	ce Depti	1 to Tep	ef Lag	rer (m) De	with to	Test	Test	Sell (Undrained Shear	Applied Normal	Undrained Young's	Undrained Shear	Internel Angle of	Dry Density	Dry Unit	Water Content	Total Suction	Bulk Unk	Vold	Degree of	Back- Coloubied	Coeff. of Earth	lastab- Rity	SPT Depth	Data	Smann/	Location	Comments	Assumed Constants
Ne.	North.	East.	(m) (A)	n Kerw	icit Sa	ad I	Lower of I	Layer (m)	Туре	Depth (m)	Tested	Strength ou (kPs)	Street (kPa)	Modulus (MPs)	Strongth cu (kPa)	Friction (degrees)	(⊮ m3)	Weight (kN/m3)	(%)	(FF)	Weight (<u>kN/m3</u>)	Rotio	Caturation (%)	Specific Gravity	Pressure at Rest	Index (%)	(=)	N	Year			
		ata See				Conp	ell Wagner	<u> </u>											<u> </u>						r	r			5-/1980	\$2 - 90 Piris St.		Specific
290	32438	80912	45.5	0 1.7				<u>>6.0</u>	SPLT SPLT	2.93	KAL			<u>73</u> 44	<u> </u>		<u> </u>					╞──┤										Gravity,
290	32438	81250	47.7	0 3.0		-+-	;	11.6	DST	4.08	KAL	100	72				1.47	14.42	30.0		18.75	0.84	96.80						W/1972	TAB Building, Fould St.		G=
291	32219	81250	47.7	0 3.0		_	>	>11.6	DST	5.28	KA.	125	100				1.44	14.13	31.0		18,51	0.88	95.66			┼──┤						<u></u>
292	32204	81279	47.9	0 2.2		-+		>7.6	DST	3.48	KA.		<u>63</u>				1.73	16.97	17.3		19.91	0.56	83.31						W/1973	Anest Building, North Tos.		
293	32796	80491	39.4					8.2	DST	6.18	KA.	149	130				1,87	18,34	15.8		21.24	0.44	96.11									
293	32796	80491	39.4	0 0.0				8.2	DST	7,68	KA	100	158				1.51	14.81	26.5		18.74	0.72	90.79	· · ·								
294	32794	80517	39.7	0 0.0				8.6	DST	6.18	K/L	. 179	129				1.77	14.02	42.2		18.60	1.13	101.19	2.74	<u> </u>	<u>├</u>						Test Types:
295	32768	80510	40.0	0 00	<u>-</u>			8.2	DST	3.08	TI.	105	67				1.36	13.34	36.5		18.21	0.99	100.02	2,70								SPLT = Screw Plate
295	32768	80510	40.0	0 0.0				8.2	DST	4.68	KA.	149	96				1.36	13.34	36.4		18.29	0.99	99.75		ļ	↓ _						Land Tool.
295	32768	80510	40.0	0.0				8.2	DST	6.18	K/L	160	130				1.33	13.05	37.4		17.93	1.03	96,03			┟──╁						Procession Test.
295	32768	80510	40.0	0 0.0				<u>8.2</u>	DST	7.68	KA.	186 91	35				1.33	13.05	36.4		17.80	1.03	95,41									CPT = Cons Penstration
296	32806	8052	37.9	0 0.0				5.9	DST_	3.06	KA	162	67				1.41	13.83	33.4		18.51	0.91	99 ,75		ļ							Test. Tillia - Triania)
296	32808	8052	37.9	0 0.0				5.9	DST	4.68	KL	215	96				1.68	16.48	22.3		20,16	0.61	99.17 104.61	2.81					\$/1970.1	Kine William St.		Unconsolidend, Undrained
297	32597	80594	45.4	0 21		+		14.0	<u>D5T</u>	4.38	K/L	134	72				1.43	14.03	32.1		18.53	0.89	97.59									test with # stages.
297	32597	80594	45.4			-+	<u> </u>	14.0	DST	7.08	KAL	177	121				1.44	14.13	31.3		18.55	0.88	96.58									TCD# = Triazial,
297	32597	80594	45.4	0 21				14.0	DST	8.58	K/L	199	146				1.38	13.54	34.2	 	18.17	0.96	96.54		ļ							the with # strang
297	32597	80594	45.4	0 2.1		_		14.0	DST	10.58	K/L	203	175	ļ			1.44	14,13	35.5		18.52	0.96	100.21	2.71	<u> </u>				\$/1970.1	Greateli St.		TUC = Triazial,
298	32538	80786	44.6		+ 7	.6	9.5	15.8	DST	4,38	x	134	105				1.44	14,13	31.4		18.56	0.88	96.89									Unconfined Compression
298	32538	80786	44.6	0 24	1 7	.6	9.5	15.8	DST	11.18	L	172	185				1.39	13.64	32.9		18.12	0.94	94.25		<u> </u>	├ ───┤						Test.
298	32538	80780	44.6	0 24	7	.6	9.5	15.8	DST	13.18	L	192	214			ļ	1.52	14.91	27.2		18.97	0.78	94.60			}}						LIST - DEVEL SAME TONC
298	32538	80780	44.6	0 24	7	.6	9.5	15.8	DST	14.58	L	292	214			<u> </u>	1.52	14.01	27.6		19.03	0.78	95.99									1
299	32446	80795	45.5	0 3.0				>12.5	DST	6.48	KAL	139	\$8				1.52	14.91	30.8	<u> </u>	19.50	0.78	107.12	2.86								Sensons:
299	32446	80799	45.5	0 3.0	,		,	>12.5	DST	12.58	K/L	220	150				1.43	14.03	32.0	 	18.52	0.89	97.29		ł	<u> </u>			en 101	Darahlin Os		S = Summer
300	32142	80484	44.6	0 1.5	; 10	0.4	11.6 >	>15.5	DST	1.58	K	57	34				1.54	15.11	24.9		18.87	0.75	89.25 96.61		<u> </u>	┼───┼			5/19/1	PRIMIN SC		W = Winter
300	32142	80484	44.6	0 1.5		0.4	11.6 >	>15.5	DST	<u>3.78</u>	K I	<u>72</u> 117	03				1.43	14.03	33.4		18.71	0.89	101.54	2.74	1							Sp = Spring
300	32142	80484	44.6	0 1.3		0.4	11.6	>15.5	DST	7.38	x	139	121	· · · · · · · · · · · · · · · · · · ·			1.41	13.83	32.5		18,33	0.91	95.91			\square						
300	32142	80484	44.6	0 1.5	5 10	0.4	11.6 >	>15.5	DST	8,88	x	154	150				1.36	13.34	37.6		18.36	0.99	103.04	2.78								
300	32142	80484	44.6	0 1.5		0.4	11.6 >	>15.5	DST	13.48		215	215	<u> </u>			1.62	14.42	30.1		19.76	0.84	97.13									
300	32142	80484	44.6	0 1.2	<u>} "</u>	0.4	11.0 2	>7.9	DST	2.98	KAL	$\frac{n}{n}$	53				1.31	12.85	37.5		17.67	1.06	95.42									
301	32199	8046	44.3	0 0.0	5			>7.9	DST	4.06	K/L	93	63				1.38	13.54	35.3		18.32	0.96	99.64									
301	32199	8046	44.3	0 0.0				>7.9	DST	7.98	K/L	144	102	 -			1.46	14.32	30.5		18.07	0.85	96.20						W/1971	Brougham PL, Nth. Adl.		
302	34297	8065	46.6	0 3.4		-+		10.7	DST	7.58	KA.	153	121				1.65	16.19	20.8	1	19.55	0.64	88.25							-		
303	34312	8062	47.1	0 3.0	51	+		8.2	DST	3.08	KA	110	59			[1.46	14.32	31.5	L	18.83	0.85	100.14	2.70		↓						
303	34312	8062	47.1	0 3.0	>			8.2	DST	6.98	KAL	182	114	ļ	<u> </u>		1.57	15.40	26.5	<u> </u>	19.48	0.72	99.41 101.42	274					5-/1972	Kine William St.		
304	32574	8056	44.7	0 2.7	<u> </u>			13.6	DST	4.98	K/L KA	62	<u> </u>			<u>+</u>	1.38	13.54	34.3	<u>t</u>	18.18	0.96	96.82		<u>t</u>							
304	32574	8056	44.7	0 2	;			13.6	DST	7.88	KAL	158	87				1.39	13.64	34.2		18.30	0.94	97.98		Į	T						
304	32574	\$056	44.7	0 2.	1			13.6	DST	9.88	K/L	206	119	ļ	ļ	<u> </u>	1.38	13.54	34.6		18.22	0.96	97.67		 	┝──┦						
304	32574	8056	44.7	0 2.1	<u>_</u>			13.6	DST	11.98	KA.	187	158	 		 	1.39	13,04	1 33.1	+	19.13	+ <u>*. <u>*</u>* </u>	79.83	<u> </u>	L					Kingston Tce., Nth. Adl.		
305	34688	8122	33.		<u>"</u>	-+	<u> </u>	>15.5	DST	1.88	KAL	57	36				1.36	13.34	36.0	1	18.14	0.99	98.65						A/1972	King William St.		
306	32425	8064	44.9	0 0.0			<u> </u>	>15.5	DST	3.28	KA.	96	59				1.47	14.42	31.1		18.91	0.84	100.35	2.71		\vdash						
306	32425	9064	5 44.5	0 0.0		$-\top$		>15.5	DST	4.78	KA	134			<u> </u>	<u> </u>	1.43	14.03	32.9	1	18.64	0.89	100.02	2.70	↓							
306	32425	8064	s 44.9	0.0	<u>-</u>		<u> </u>	>15.5	DST	10.48	KA-	201	202	<u> </u>	<u> </u>	-	1.49	14.62	30.2		19.03	0.81	100.41	2.71	1							
1200	32425	8064	5 44.9	<u>NU 0.1</u> NO 0.1			+	>15.5	DST	13.68	KAL	239	239				1.44	14.13	31.6		18.59	0.88	97.51								l	
307	32372	8071	45.5	50 3.0	0			>6.1	DST	4.18	K/L	86	58	ļ	ļ	ļ	1.59	15.60	26.7		19.76	0.70	103.26	2.76		├			S/1972	Pinie SL		
307	32372	8071	45.5	50 3.0				>6.1	DST	5.38	KAL	110	72	·		 	1.44	14.13	30.2	+	18.66	0.88	100.41	2.71	<u> </u>							
306	32338	8074	2 46.0	2		0.4	11.3 :	>13.7	DST	4.78	K K	101 158	114	<u> </u>	†		1.47	14.42	30.4		18.80	0.84	98.10		1							
308	32338	8074	2 46.0	$\frac{2}{2}$; ;	0.4	11.3	>13.7	DST	8.58	R	192	163				1.44	14.13	33.1	1	18.80	0.88	102.14	2.75	h		· · ·					
308	32338	8074	46.0	2	<u>i</u>	0.4	11.3	>13.7	DST	13.68	L	225	216	L	ļ	 	1.47	14.42	30.5		18.82	0.84	98.42			┟──┤			A/1072			
309	32376	8073	45.9	50 1.1				>6.5	DST	2.36	KA	67	43	<u> </u>	·	+	1.39	14 12	32.8	+	18.91	0.85	101.73	2.74	1							
309	32376	8073	<u>} 45.5</u>			+		>6.3	DST	2.78	KA.	81	49				1.39	13.64	32.2		18.03	0.94	92.25						Sp/1971	King William St.		
310	31638	\$067	5 44.4	0 2	1		<u> </u>	>9.3	DST	5.88	KA	101	105				1.41	13.83	34.1		18.55	0,91	100.63	2.72	 	↓ • ↓						
1 110	11410				. 1				DST	0.18	KA.	172	153	1	1	1	1.35	13.24	36.4	t	18.06	1.00	95.28	L	1						<u> </u>	1

Table C.7Data from Connell Wagner (SA) Pty. Ltd.

Table C.8Data from Kinhill Engineers Pty. Ltd.

							D	· · · · · ·	1		Kindenland	Canfining	Tindenland	Tindepland	Internal	Der	Dry	Water	Total Bul		Degree	Beck	Ceeff.	Instab	SPT	Data	-		r	
	AMG	CHAL	BUTINCE DT	Debri 10			Battem	Test	Teat	Laver	Sheer	Pressure	Yanas's	Sheer	Angle of	Density	Unit	Content	Suction Uni	Veit	4	Calculated	f of Earth	i i i i i i i i i i i i i i i i i i i	Depth		Season/	Location	Comments	Assumed Constants
Na	North.	Real	5	Kerwich	Sand	Lower	ef Løyer	Туре	Depth	Turind	Strungth	(kPa)	Medalme	Strungth	Triction	(¥m3)	Weight	(%)	(pP) Weig	t Rati	Saturation	Specific	Pressure	Index	(=)	N	Year			and Legend
1			(AHD)				(111)		ക		su (killa)		()((Ph))	en (kPa)	(degreet)		(kN/m3)		(kN/=	<u>n</u>	(%)	Grevity	at Rest	(%)	<u> </u>	<u> </u>	<u> </u>			
	D	ata Source			Kin	hill Ragio															<u> </u>	·				.	· · · · · ·			
312	33001	81076	40.05	N/B																		<u> </u>		<u> </u>				Berr Smith Library Stage 3		Specific
313	33029	81032	39.91	N/B_					L										l				+			 				Gravity,
314	33034	80330	25.70	N/B																			+	 		╉────		Adelaide Perkval Course-Drame Th.		0-
315	32436	80856	45.21	2.3			13.7	TUU3	3.20	KA.	71	69	2	76		7'20	-12:24	32.0	18.0	4.97	91.33	 		┨────	<u> </u>	ł	\$/19/3	National Bank Coolie, Piris St.		2.7
										I I	86	207					+				+	 			<u> </u>	 	-			
											90	414						20.2	10.1	0.76	100.04	2.20	+			1	1			· · · ·
315	32436	80856	45.21	2.3			13.7	1003	4.72	KA.	133	103		124	- 2	1.21	-19.91	67.6			1 10002	1 */v	+			<u>+</u>	-		· · · · · · · · · · · · · · · · · · ·	
			ļ						 		150	276			-							1	<u> </u>	1	ł	+	1			
					ļ				1		160	332	-	207		1 58	15.50	26.0	19.5	071	99.03	1				<u> </u>	1			
315	32436	80856	45.21	2.3	 		13.7	TUU3	6.25	K/L	219	158		<i>a</i> ur			12.24				17.07		-		t	<u>†</u>	1			
					<u> </u>				1		240	4/0									1		1				1			f
					↓				2.22	1 10	217	128		207	1	1.44	14.13	32.4	18.7	0.84	99.95		1	-			1			
315	32436	80856	45.21	23			13.7	1003	1.11	N/L	217	276								-	1						1			
				<u> </u>					<u> </u>		231	552									1		1			1	1			
1.10	33436	-	46.31	2.2			137	11113	0 30	XA.	255	172		248	0.6	1.47	14.42	31 <i>A</i>	18.9	0.84	101.32	2,73	1]			
313	20.00	0.0.0	73.61						1	1	262	345						_												
			<u> </u>		1						265	690																		
315	32436	80856	45.21	23			13.7	TUU3	12.34	KA	234	241	4	234	0	141	13.83	33.5		0.91	98.86	L					1			
1.12					1						228	483								<u> </u>	<u> </u>		ļ							
			t		1						228	758		· ·						+						h	<u> </u>			
316	32415	80846	45.21	2.7			14.9	TUU3	3.20	K/L	103	69	3	103	1.	1.56	15.30	26.2		0.73	96.80	<u> </u>					\$/1973			Test Types:
											115	207								+									·····	SPLT = Screw Piate
				1				L	4		121	414	<u> </u>							-	P7 03	t	†	├	<u> </u>	<u> </u>				Load Test.
316	32415	80846	45.21	2.7	1		14.9	TUU3	4.72	KA	93	103	4	90	1.5	1.48	14,52	49.9	15.5	0.82	11.93	<u> </u>	ł			1				SEPT = Self Boring
			L	 	 			<u> </u>	+	<u> </u>	105	276		i							<u> </u>		<u> </u>	<u> </u>		I				Producementer Test.
			1	<u> </u>	 				1	<u>-</u> -	112	352		149	1.0	145	14.22	31.0	18 74	0.14	99.91	i	1		<u>-</u>	1				
316	32415	80846	45.21	27	╡───	 	14.9	1 1003	6.25		160	138		179	- 1.0	1,72	-17.64	21.7		1	- <u> </u>	İ	r			1			<u> </u>	
		L	<u> </u>	ł	╉────			 			104	4/0								1			1			1				Income Institut,
-			1.000			1 .	14.	77175	1 7 777	1 4 4	200	132	-	200	1	1.41	13.83	33.9	18.52	0.91	100.04	2.70	1							the with it shaws
316	32415	80546	45.21	27	+	<u>↓</u>	14.9	1003	1.11		214	276														1				TCD# a Triazial
			╂	<u> </u>	+				1		219	552														l				Consolidend, Drained
116	22416	-	45.21	1 27	1		14.0	THUS	9.30	KA.	78	172	7	76	0.5	1.43	14.03	33.0	18.60	0.89	100.33	2.71							Piasure failure?	wet with # stages.
1310	34912	80840	43.21		<u> </u>		- 17.2	1005	1	- A	01	345																		TUC = Triazial,
			<u> </u>						1		112	690																		Unconfined Compression
316	32415	20846	45.21	27	1		14.9	τυυз	12.34	K/L	178	241	6	178	0	1.39	13.64	34.8	18.36	0.94	99.70				_					Test.
1.0				+							178	483								_										DST = Direct Shear Test.
				1	1						183	758											l							
317	31227	79744	40.40	1.5			6.7													<u> </u>								Trades Hall, South Tce.		
318	31210	79712	40.20	3.0			8.2					ļ							·											Sectors
319	34220	80392	46.20	4.1			7.9		1			-	L	ļ						_								52 Brougham PL		S = Summer
320	32300	80707	40.00	3.4	9.6	10.6	17.1		1				ļ							+								Car. Pine St. & Exchange Pl.		A = Autuma
			42.62								1																			W = Winter
321	32456	80702	45.60	3.0	10.5	11.9	15.8		+		I	ļ	ļ	ļ																
321 322	32456 33050	80702 80450	49.69 45.60 26.31	3.0 N/E	10.5	11.9	15.8		<u> </u>											1								Pestival Theere		Sp = Spring
321 322 323	32456 33050 32725	80702 80450 80871	45.60 26.31 45.00	3.0 N/E 2.4	10.5	11.9	15.8																					Pestival Theere Woolworths, Rundle Mail		Sp = Spring
321 322 323 324	32456 33050 32725 32779	80702 80450 80871 80866	49.69 45.60 26.31 45.00 44.70	3.0 N/E 2.4 2.7	10.5	11.9	15.8 12.4 12.5				· · · · · · · · · · · · · · · · · · ·																	Pestival Theetre Woolworths, Rundle Mall		Sp = Spring
321 322 323 324 325	32456 33050 32725 32779 31566	80702 80450 80871 80866 80727	49.69 45.60 26.31 45.00 44.70 44.30	3.0 N/E 2.4 2.7 4.0	10.5	11.9	15.8 12.4 12.5 >15.2																					Petival Thesite Woolworths, Rundle Mall Mercantile Chofits, Car. King William & Halifas, Sa.	R(50)	So = Spring
321 322 323 324 325 326	32456 33050 32725 32779 31566 31570	80702 80450 80871 80866 80727 80748	42.62 45.60 26.31 45.00 44.70 44.30 44.20	3.0 N/E 2.4 2.7 4.0 4.0	10.5 10.7 10.7 11.0	11.9 11.7 12.6	15.8 12.4 12.5 >15.2 >15.2																					Pesival Theetro Woolworths, Rundle Mall Morcantile Cardise, Car. King William & Halifax Su. ANZ Beak: Car. King William	E(50)	So = Spring
321 322 323 324 325 326 326	32456 33050 32725 32779 31566 31570 32551	80702 80450 80871 80866 80727 80748 80586	49.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62	3.0 N/E 2.4 2.7 4.0 4.0 5.0	10.5 10.7 11.0	11.9 11.7 12.6	15.8 12.4 12.5 >15.2 >15.2 >10.5																					Pesival Thears Woolworth, Runde Mall Mercantile Caelite, Car. King William & Halifas Su. ANZ Bank, Car. King William & Carrie Su,	E(50)	So = Sprjag
321 322 323 324 325 326 327 328	32456 33050 32725 32779 31566 31570 32551 32563	80702 80450 80450 80871 80866 80727 80748 80586 80586 80586	42.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.62 44.50 42.10	3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1	10.5 10.7 10.7	11.9 11.7 12.6	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9																					Pesival Theare Woolworth, Runde Mall Mercantile Cardis, Car. King William & Halifax Su. ANZ Bank, Car. King William & Carrie Ste. 23-25 Laigh St.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 329	32456 33050 32725 32779 31566 31570 32551 32563 32588 3263	80702 80450 80871 80866 80727 80748 80586 80576 80402 80600	42.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.62 44.50 42.10	3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1 3.4	10.5 10.7 11.0 5.8	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5	TUU3	4.15	KA	151	69	23	153	1	1.42	13.93	33.0	18.53	0.90	98.85						A/1982	Pesival Theare Woolworths, Runde Mall Mercantile Cardits, Car. King William & Halifax Su. ANZ Bank, Car. King William & Carrie Sts. 23-25 Leigh St. Mutual Health Building	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330	32456 33050 32725 32779 31566 31570 32551 32563 32588 32463	80702 80450 80450 80871 80866 80727 80748 80586 80576 80586 80576 80402 80402	42.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.62 44.62 44.50 42.10	3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1 3.4	10.5 10.7 11.0 5.8	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5	TUU3	4.15	KAL	151	69 138	23	153	1	1.42	13.93	33.0	18.53	0.90	91.85						A/1982	Pesival Thears Woolworths, Runde Mall Mercantile Cardits, Car. King William & Halifax Su. ANZ Bank, Car. King William & Carrie Su, 23-25 Leigh St. Mutual Heakh Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330	32456 33050 32725 32779 31566 31570 32551 32563 32588 32463	80702 80450 80450 80871 80866 80727 80748 80586 80576 80402 80402	42.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.62 44.50 42.10	3.0 3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1 3.4	10.5 10.7 11.0 5.8	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5	TUU3	4.15	KAL	151 158 174	69 138 276	23	153	1	1.42	13.93	33.0	18.53	0.90	98.85						A/1982	Pesival Theory Woolworth, Rundle Mall Mercantile Caedis, Car. King William & Halfan Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330	32456 33050 32725 32779 31566 31570 32551 32563 32588 32463	80702 80450 80671 80871 80866 80727 80748 80586 80576 80402 80800	47.22 45.60 26.31 45.00 44.70 44.30 44.30 44.42 44.52 44.52 44.510	3.0 3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1 3.4 3.4	10.5 10.7 11.0 5.8	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5	TUU3	4.15	KA.	151 158 174 107	69 138 276 103	23	153		1.42	13.93	33.0 2 8 .0		0.90	98.85 95.93						A/1982	Pesival Tanatro Woolworth, Runde Mall Mercantile Cardia, Car. King William & Halifaz Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330	32455 32455 33055 32725 32779 31566 31570 32551 32563 32563 32563 32463	80702 80702 804502 80450 8071 80865 80727 80748 80586 80576 80402 80800	47.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.62 44.50 42.10 45.10	3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1 3.4 3.4	10.5	11.9	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5	TUU3	4.15	KA.	151 158 174 107 117	69 138 276 103 207	23	153	1	1.42	13.93	33.0	18.53 	0.90	98.85 95.93						A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Casilis, Car. King William & Halifaz Su. ANZ Bank, Car. King William & Carrie Sta, 23-25 Laigh St. Mutual Health Building Gawier Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330	32456 33050 32725 32779 31566 31570 32551 32563 32563 32563 32563 32463	80702 80702 80452 80452 80571 80565 80722 80585 80576 80576 80576 80576 80576 80570 80570 80570 80570	47.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.50 42.10 45.10	3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1 3.4 3.4	10.5	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5	TUU3	4.15	KA.	151 158 174 107 117 137	69 138 276 103 207 414	23	153		1.42	13.93	33.0	18.55	0.90	98.8 5 95.9 3						A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Caslies, Car. King William & Halifax Su. ANZ Bank, Car. King William & Carrie Su. 22-25 Leigh St. Mutual Health Building Gawier Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330	32456 33050 32725 32779 31566 31570 32551 32563 32263 32463 32463	80702 80702 804502 80450 80571 80565 80727 80585 80576 80576 80576 80576 80576 80576 80576 80576 80570 80500	45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.62 44.50 45.10	3.0 N/E 2.4 2.7 4.0 4.0 2.7 2.1 3.4 3.4 3.4	10.5	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5	TUU3	4.15 6.15 7.95	KA. KA.	151 158 174 107 117 137	69 134 276 103 207 414 138	23 20 35	153 103 131	1 1 2	1.42	13.93	33.0 28.0 33.0	18.55 18.55 18.66	0.90	98.85 95.93 100.33	271					A/1982	Pesival Theory Woolworth, Rundle Mall Mercantile Caedia, Car. King <u>William & Halfan Su.</u> ANZ Bash, Car. King William <u>& Cantie Su.</u> 23-25 Leigh St. Mutual Health Building Gawier Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330 330	32456 33050 32725 32779 31566 31570 32551 32563 32588 32463 32463	80702 80702 80450 80871 80865 80732 80745 80745 80745 80745 80745 80745 80800 80800	47.62 45.60 26.31 45.00 44.70 44.30 44.20 44.20 44.62 44.50 42.10 45.10	3.0 N/E 2.4 2.7 4.0 4.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	10.5	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 	TUU3	4.15 6.15 7.95	KA. KA.	151 154 174 107 117 134 157	69 138 276 103 207 414 138 276	23	153 103 131	1 2	1.42	13.93 14.81 14.03	33.0 28.0 33.0	18.53 18.55 18.96	0.90	98.85 95.93 100.33	2.71					A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Castis, Car. King William & Halifat Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Health Building Gawier Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330 330	32456 33050 32725 32779 31566 31570 32551 32563 32585 32463 32463	80702 80750 80450 80871 80865 80745 80745 80745 80745 80745 80745 80402 80800 80800	47.62 45.60 44.70 44.30 44.70 44.30 44.62 44.50 42.10 45.10 45.10	3.0 N/E 2.4 2.7 4.0 5.0 2.7 2.1 3.4 3.4 3.4 3.4	10.5	11.9 11.7 12.6 9.4	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5 	TUU3	4.15 6.15 7.95	КА. КА.	151 158 174 107 117 137 134 157 185	69 138 276 103 207 414 138 276 552	23	153	1 1 2	1.42	13.93	33.0 28.0 33.0	18.53 18.55 18.95 18.96	0.90	95.93 95.93	2.71					A/1982	Pesival Theory Woolworth, Runde Mall Mercantile Cardis, Car. King William & Hairfan Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330 330	32456 33050 32725 32779 31566 31570 32551 32563 32463 32463 32463 32463	80702 80450 8072 80450 80450 80450 80451 80586 80721 80721 80728 80721 80721 80721 80721 80721 80721 80721 80721 80800 80800 80800	47.62 45.60 26.31 45.00 44.70 44.30 44.62 44.50 44.62 44.50 45.10 45.10	3.0 N/E 2.4 2.7 4.0 5.0 2.7 2.1 3.4 3.4 3.4 3.4 2.1	10.5 10.7 10.7 11.0 5.8 	11.9 11.7 12.6 9.4 	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5 	TUU3	4.15 6.15 7.95 4.15	КА. КА. КА.	151 158 174 107 117 137 134 157 185 92	69 138 276 103 207 414 138 276 552 69	23	153 103 131		1.42 1.51 1.43	13.93 14.81 14.03 14.42	33.0 28.0 33.0 31.0	18.55 18.55 18.56 18.66 18.69	0.90	98.85 95.93 100.33 100.03	2.71					A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Casilis, Car. King William & Halifaz Su. ANZ Bank, Car. King William & Carrie Sta, 23-25 Laigh St. Mutual Health Building Cawler Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330 330	32456 33059 32725 32777 31566 31570 32551 32563 32588 32463 32463	80702 80450 80450 80450 80450 80711 80866 80772 80748 80748 80748 80748 80748 80748 80576 80402 80576 80500 80500	47.62 45.60 26.31 45.00 44.70 44.20 44.20 44.20 44.20 44.50 42.10 45.10 45.10	3.0 N/E 2.4 2.7 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1	10.5 10.7 11.0 5.8 10.7 11.0 10.7 1	11.9 11.7 12.6 9.4 10.7	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.2	TUU3 TUU3	4.15 6.15 7.95 4.15	КА. КА. КА.	151 158 174 107 117 137 134 157 185 92 99	69 138 276 103 207 414 138 276 552 69 138	23 20 35 20	153 103 131 94	1 1 2 1	1.42 1.51 1.43	13.93 14.81 14.03 14.42	33.0 28.0 33.0 31.0		0.90	98.85 95.93 100.33 100.03	2.71					A/1982	Pesival Thears Woolworth, Rundle Mall Mercantile Caedia, Car. King <u>William & Halifan Su.</u> ANZ Bash, Car. King William <u>& Cantie Su.</u> 23-25 Laigh St. Munal Health Building Gawier Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330 330	32456 33050 32725 32779 31566 31570 32551 32563 32583 32463 32463 32463	80702 80450 80450 80450 80571 80565 80723 80723 80724 80576 80472 80576 80472 80576 80472 80500 80500 80500	47.62 45.60 26.31 45.00 44.70 44.30 44.20 44.20 44.20 44.20 44.20 45.10 45.10 45.10	3.0 N/E 2.4 2.7 4.0 5.0 2.7 2.1 3.4 3.4 3.4	10.5 10.7 11.0 5.8 	11.9 11.7 12.6 9.4 10.7	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5 	TUU3	4.15 6.15 7.95 4.15	КА. КА. КА.	151 158 174 107 117 137 134 157 185 92 99 91	69 134 276 103 207 414 138 276 552 69 138 276	23	153 103 131 94		1.42 1.51 1.43	13.93 14.81 14.03 14.42	33.0 28.0 33.0 33.0 33.0		0.90	98.85 95.93 100.33 100.03	2.71					A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Caedis, Car. King William & Halifan Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 326 326 327 328 329 330 330 330 330 331	32456 33050 32725 32779 31566 31570 32551 32563 32563 32463 32463 32463 32463	80702 80450 8072 80450 80855 80711 808555 8072 8072 804702 804702 804702 80400 80400 80400	45.60 44.50 44.70 44.70 44.70 44.70 44.70 44.70 44.20 44.62 44.50 45.10 45.10 45.10 45.10 45.10	3.0 N/E 2.4 7 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1 2.1	10.5 10.7 11.0 5.8 10.0	11.9 11.7 12.6 9.4 10.7	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3 TUU3	4.15	КА. КА. КА. К.	151 158 174 107 117 137 137 137 157 185 92 99 111 138	69 138 276 103 207 414 138 276 552 69 276 552 69 138 276 110 138	23 20 20 20 20 17	153 103 131 94		1.42 1.51 1.43 1.47	13.93 14.81 14.03 14.42 13.83	33.0 28.0 33.0 31.0 34.0	18.53 18.55 18.66 18.66 18.66	0.90	98.85 95.93 100.33 100.03	2.71					A/1982 A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Castis, Car. King William & Halifat Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Health Building Gawier Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 330 330 330 330 330 330 330	32455 33059 32725 32772 31566 31570 32551 32563 32588 32463 32463 32463 32463	80702 80450 80450 80450 80871 80586 80576 80576 80576 80576 80576 80576 80570 80570 80570 80500 80500 80500 80500 80500	47.62 45.60 26.31 45.00 44.70 44.30 44.30 44.20 44.62 44.62 44.50 45.10 45.10 45.10	3.0 N/E 2.4 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 3.4 2.1	10.5 10.7 10.7 11.0 5.8 10.0 10.0	11.9 11.7 12.6 9.4 10.7 10.7	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.5 >14.2	TUU3 TUU3	4.15	KAL KAL KAL K	151 158 174 107 117 137 134 157 185 92 99 99 111 138 149	69 138 276 103 207 414 138 276 552 69 138 276 552 69 138 276 110 221	23 29 35 20 17	153 103 131 94 141	1	1.42 1.51 1.43 1.47	13.23 14.81 14.03 14.42 13.83	33.0 28.0 33.0 33.0 31.0 34.0		0.90	98.85 95.93 100.33 100.03 100.34	2.71					A/1982	Pesival Theory Woolworth, Runde Mall Mercantile Cardis, Car. King William & Haifan Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = 3pring
321 322 323 324 325 326 326 327 328 329 329 329 330 330 330 330	32456 33059 32725 32777 31566 31570 32551 32563 32588 32463 32463 32463 32463	80702 80450 80450 80450 80450 80450 80450 80450 80712 80748	45.60 26.31 45.60 44.70 44.30 44.20 44.20 44.20 44.20 44.50 45.10 45.10 45.10	3.0 N/E 2.4 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1 2.1	10.5 10.7 10.7 11.0 5.8 10.0 10.0 10.0	11.9 11.7 12.6 9.4 10.7 10.7	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3	4.15	KAL KAL KAL KAL	151 158 174 107 117 137 134 157 185 92 99 99 111 138 149 170	59 138 276 103 207 414 138 276 552 69 134 276 110 221 414 138	23 23 20 35 20 17	153 103 131 94 141		1.42 1.51 1.43 1.47 1.41	13.93 14.81 14.03 14.42 13.83	33.9 28.0 33.0 31.0 34.0 35.0	18.55 18.56 18.66 18.69 18.69 18.69 18.69 18.69 18.69 18.59 18.60 18.59 18	0.90	98.85 95.93 100.33 100.33 100.34 100.27	2.71					A/1982	Perival Theory Woolworth, Rundle Mall Mercantile Coeffis, Car. King <u>William & Halifas Su.</u> ANZ Bash, Car. King William <u>& Carrie Su.</u> 23-25 Laigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 326 326 327 328 329 329 329 329 329 330 330 330 330 331	32456 33050 32725 32777 31566 31570 32551 32563 32563 32463 32463 32463 32463	80702 80450 80450 80450 80571 80576 80748 80576 80457 80576 804572 80576 804572 80576 804572 805706 80500 80500 80500 80510	45.60 44.76 44.76 44.70 44.70 44.70 44.70 44.70 44.70 44.70 44.70 44.70 44.70 44.70 44.70 44.70 45.10 45.10 45.10 45.10	3.0 N/E 2.4 2.7 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1 2.1 2.1	10.5 10.7 11.0 5.8 10.7 11.0 10.7 10.7 10.7 10.0 10.0 10.0 10.0	11.9 11.7 12.6 9.4 10.7 10.7	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3 TUU3	4.15 7.95 4.15 7.95 7.95	KAL KAL KAL K	151 158 174 107 117 137 134 155 92 99 91 111 138 92 99 111 138 149 170 190	69 138 276 103 207 414 138 276 552 552 562 69 138 276 138 276 110 221 441 138	23 20 35 20 17 17	153 103 131 94 141 192		1.42 1.51 1.43 1.47 1.41 1.39	13.93 14.81 14.93 14.42 13.83 13.64	33.0 28.0 33.0 31.0 34.0 35.0		0.90	98.85 95.93 100.33 100.03 100.03 100.34	2.71					A/19#2	Pesival Theory Woolworth, Rundle Mall Mercantile Chefits, Cur. King William & Hafira Su. ANZ Bank, Cur. King William & Carrie Su. 22-25 Leigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 326 326 326 327 328 329 320 329 320 320 320 320 320 320 320 320 320 320	32456 33050 32725 32773 31566 31570 32551 32563 32583 32583 32463 32463 32463 32463 32463	80702 80450 8072 80450 80972 809555 8072 8072 804700 80000 80000	47.62 45.60 26.31 45.00 44.70 44.30 44.20 44.62 44.50 45.10 45.10 45.10 45.10 45.10	3.0 N/E 2.4 7 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1 2.1 2.1	10.5 10.7 10.7 11.0 5.8 10.0 10.0 10.0 10.0	11.9 11.7 12.6 9.4 9.4 10.7 10.7	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3 TUU3 TUU3	4.15	КЛ. КЛ. К. К.	151 158 177 107 117 137 138 157 185 92 92 99 111 138 149 170 190 203	69 138 276 103 207 414 138 276 552 69 110 221 411 138 276 110 221 441 138 276	23 20 20 20 20 17 17	153 103 131 94 141 192		1.42 1.51 1.43 1.47 1.41	13.93 14.81 14.03 14.42 13.83 13.64	33.0 28.0 33.0 31.0 34.0 35.0	18.53 18.53 18.55 18.66 18.66 18.66 18.54 18.54	0.90	98.85 95.93 100.33 100.03 100.03 100.27	2.71					A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Castis, Car. King William & Halifat Su. ANZ Bank, Car. King William & Carrie Su. 23-25 Leigh St. Mutual Heath Building Gawier Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 329 329 329 329 329 320 320 320 320 320 320 320 320 320 320	32456 33059 32773 32773 31566 31570 32563 32588 32463 32463 32463 32463 32463 32463	80702 80750 80750 80450 80450 80871 80556 80772 80748 80576 80576 80576 80576 80576 80570 80500 80500 80500 80500 80510 80510	47.62 45.60 26.31 45.00 44.70 44.30 44.30 44.20 44.62 44.62 44.50 45.10 45.10 45.10 45.10	3.0 N/E 2.4 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 3.4 2.1 2.1 2.1	10.5 10.7 10.7 11.0 5.8 10.0 10.0 10.0 10.0 10.0 10.0	11.9 11.7 12.6 9.4 9.4 10.7 10.7 10.7	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.5 >14.2 >14.2 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3 TUU3 TUU3	4.15	КЛ. КЛ. КЛ. КЛ. К. К.	151 158 174 177 117 137 134 157 185 92 99 99 111 138 149 111 138 149 170 190 205 231 71	69 138 276 100 207 414 138 276 552 69 138 276 110 221 411 138 276 552 69	23 23 20 20 20 17 17 17 26	153 103 131 94 141 192 73		1.42 1.51 1.43 1.47 1.47 1.41 1.39	13.93 14.81 14.03 14.42 13.83 13.64	33.0 28.0 33.0 31.0 34.0 35.0 29.0	18.53 18.55 18.96 18.66 18.69 18.54 18.54 18.41	0.90	95.93 95.93 100.33 100.03 100.27 96.42	2.71					A/1982 A/1982	Pesival Theory Woolworth, Runde Mall Mercantile Cashis, Car. King <u>William & Halifan Su.</u> ANZ Bank, Car. King William <u>& Carrie Su.</u> 23-25 Leigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 329 329 329 329 329 329 329 329 329	32455 33059 32725 32775 31566 31570 32551 32563 32588 32463 32463 32463 32463 32463	80702 80450 80450 80450 80450 808271 80586 80772 80748 80748 80748 80748 80748 80748 80748 80748 80748 80748 80800 80800 80810 80810 80810	45.60 26.31 45.60 44.70 44.30 44.30 44.20 44.20 44.20 44.50 45.10 45.10 45.10 45.10 45.10 45.10	3.0 N/E 2.4 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1 2.1 2.1 2.1 2.1 2.1	10.5 10.7 10.7 11.0 5.8 	11.9 11.7 12.6 9.4 10.7 10.7 10.7 10.7	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.2 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3 TUU3 TUU3	4.15	КЛ. КЛ. КЛ. КЛ. К. К.	151 158 174 107 117 137 134 155 185 92 99 99 99 99 1111 138 149 170 190 205 231 71	59 138 276 103 207 414 138 276 552 69 138 276 552 110 221 441 138 276 552 552 552 138	23 29 35 20 17 17 17 17 36	153 103 103 131 141 141 192 73		1.42 1.51 1.43 1.47 1.47 1.41 1.39 1.49	13.23 14.81 14.03 14.42 13.83 13.64 14.62	33.0 28.0 33.0 31.0 35.0 29.9	18.55 18.55 18.56 18.66 18.66 18.69 18.69 18.59 18	0.90	98.85 95.93 100.33 100.33 100.34 100.27 95.42	2.71					A/1982 A/1982	Perival Theory Woolworth, Rundle Mall Mercantile Coeffic, Car. King <u>William & Halifan Su.</u> ANZ Bash, Car. King <u>William</u> <u>& Cantie Su.</u> 23-25 Laigh St. Mutual Health Building Gawler Pl.	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 329 329 329 329 329 329 329 320 329 329 320 329 320 320 320 320 320 320 320 320 320 320	32456 33050 32725 32777 31566 31570 32551 32563 32563 32463 32463 32463 32463 32463 32463	80702 80450 80450 80450 80450 805716 80738 80738 80738 80738 80738 80738 805716 80472 805716 80472 805706 80510 80810 80810 80810	45.60 44.50 44.50 44.30 44.30 44.30 44.30 44.20 44.20 44.20 44.20 44.20 44.20 44.20 45.10 45.20 45	3.0 N/E 2.4 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1 2.1 2.1 2.1 2.1	10.5 10.7 11.0 5.8 10.0 10.0 10.0 10.0 10.0 10.0 10.0	11.9 11.7 12.6 9.4 9.4 10.7 10.7 10.7 10.6	15.8 12.4 12.5 >15.2 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.2 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3 TUU3 TUU3 TUU3	4.15	KAL KAL KAL KAL K	151 158 174 107 117 137 134 157 185 92 99 91 111 138 149 170 190 205 231 71 179 92	69 138 276 103 207 414 138 276 552 69 138 276 138 276 138 276 552 441 138 276 552 69 138 276 552 552	23 20 35 20 17 17 17 36	153 103 131 94 141 192 73		1.42 1.51 1.43 1.47 1.41 1.39 1.49	13.93 14.81 14.03 14.42 13.83 13.64	33.0 28.0 33.0 31.0 34.0 35.0 29.0		0.90	98.85 95.93 100.33 100.03 100.03 100.27 96.42	2.71 2.71 2.71					A/1982 A/1982	Pesival Theory Woolworth, Runde Mall Mercantle Chefis, Cur. King <u>William & Halfan Su.</u> ANZ Bank, Cur. King William <u>& Cantie Su.</u> 23-25 Leigh St. Mutual Health Building Gawier Pl	E(50)	Sp = Spring
321 322 323 324 325 326 327 328 329 329 329 320 320 320 320 320 320 320 320 320 320	32456 33050 32725 32773 31566 31570 32551 32563 32583 32463 32463 32463 32463 32463 32463 32463 32463 32463 32463	80702 80450 8072 80450 80450 80575 8072 8072 8072 8072 8072 8072 8072 8072	47.62 45.60 26.31 45.00 44.70 44.30 44.20 44.20 44.20 44.20 44.20 45.10 45.10 45.10 45.10 45.10 45.10 45.10	3.0 N/E 2.4 4.0 4.0 5.0 2.7 2.1 3.4 3.4 3.4 2.1 2.1 2.1 1.9 1.9	10.5 10.7 10.7 11.0 5.8 	11.9 11.7 12.6 9.4 9.4 10.7 10.7 10.7 10.7	15.8 12.4 12.5 >15.2 >10.5 >9.9 11.7 >14.5 >14.5 >14.5 >14.5 >14.2 >14.2 >14.2 >14.2 >14.2	TUU3 TUU3 TUU3 TUU3 TUU3 TUU3 TUU3 TUU3	4.15	KAL KAL KAL KAL KAL KAL KAL KAL KAL KAL	151 158 174 107 117 137 137 137 137 137 137 137 137 13	69 138 276 103 207 414 138 276 552 69 138 276 110 221 441 138 276 552 69 138 276 103	23 20 20 35 20 17 17 17 36 30	153 103 131 131 141 141 192 73 73		1.42 1.51 1.43 1.47 1.41 1.39 1.49	13.93 14.81 14.03 14.42 13.83 13.64 14.62 14.13	33.0 28.0 33.0 31.0 34.0 35.0 29.0 32.0	18.53 18.55 18.65 18.65 18.65 18.65 18.85 18.54 18.54 18.54 18.55 18	0.90	98.85 95.93 100.33 100.03 100.03 100.27 95.42 98.74	2.71 2.70 2.71 2.71					A/1982 A/1982	Pesival Thears Woolworth, Runde Mall Mercantile Caedia, Car. King William & Halifat Su. ANZ Bank, Car. King William & Cantie Su. 23-25 Leigh St. Mutual Health Building Gawler PL	E(50)	Sp = Spring
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